POLITECNICO DI TORINO ESAMI DI STATO PER L'ABILITAZIONE ALL'ESERCIZIO DELLA PROFESSIONE DI INGEGNERE DELL'INFORMAZIONE IUNIOR

I Sessione 2018 - Sezione B Settore dell'Informazione

Prova PRATICA del 23 luglio 2018

Il Candidato svolga il seguente tema proposto.

L'elaborato prodotto dovrà essere stilato in forma chiara, ordinata, sintetica e leggibile. La completezza, l'attinenza e la chiarezza espositiva costituiranno elementi di valutazione.

Progettare un amplificatore di condizionamento atto ad interfacciare un sensore di temperatura di tipo NTC ad un convertitore A/D.

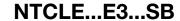
Le specifiche di progetto sono le seguenti:

- Valore di resistenza dell'NTC a 25 gradi centigradi: 10 kOhm
- Dinamica di ingresso del convertitore A/D: 2,5 V
- Tensione di alimentazione del circuito: 3,3 V
- Intervallo di temperatura in ingresso: 0 100 gradi centigradi

Al termine del progetto, il candidato descriva le specifiche dettagliate del sistema ottenuto (precisione, consumi, ecc.).

Materiale:

- Datasheet NTC
- Datasheet convertitore A/D
- Datasheet amplificatore operazionale





Vishay BCcomponents

NTC Thermistors, 2-Point Mini Chip Sensor, Flexible Leads



QUICK REFERENCE	DATA	
PARAMETER	VALUE	UNIT
Resistance value at 25 °C	3K to 10K	Ω
Tolerance on R ₂₅ -value	± 2.18	%
B _{25/85} -value	3977	K
Tolerance on B _{25/85} -value	± 0.75	%
Operating temperature range at zero dissipation	- 40 to + 125	°C
Accuracy for T measured between 0 °C and 50 °C	± 0.5	°C
Maximum power dissipation at 55 °C	100	mW
Minimum dielectric withstanding voltage (RMS) between leads and coating	500	V
Climatic category (LCT/UCT/days)	40/125/56	
Weight	≈ 0.2	g

FEATURES

- Accuracy of 0.5 °C between 0 °C and 50 °C
- Small diameter
- High stability over a long life
- Long and flexible leads for special mounting or assembly requirements
- AEC-Q200 qualified
- Compliant to RoHS Directive 2002/95/EC and in accordance to WEEE 2002/96/EC





RoHS COMPLIANT

APPLICATIONS

 Temperature measurement, sensing and control in automotive, industrial and consumer electronic equipment

DESCRIPTION

These negative temperature coefficient thermistors consist of a mini-chip soldered between two EFTE insulated (LE300) or non-insulated (LE201) nickel leads and coated with a solid ochre epoxy lacquer.

PACKAGING

The thermistors are packed in cardboard boxes; the smallest packing quantity is 1000 units.

MARKING

The body is colored with ochre lacquer and not marked.

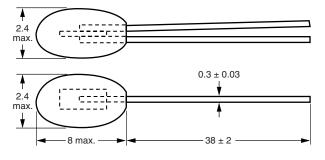
MOUNTING

By soldering in any position.

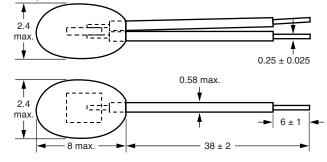
ELECTRICAL DATA AN	ID ORDERING INFORMAT	TION	
R ₂₅ -VALUE (kΩ)	B _{25/85} -VALUE (K)	SAP MATERIAL AND ORDERING NUMBER NTCLE201E3	OLD 12NC CODE 2381 645
3	3977	302SB	10302
5	3977	502SB	10502
10	3977	103SB	10103
R ₂₅ -VALUE (kΩ)	B _{25/85} -VALUE (K)	SAP MATERIAL AND ORDERING NUMBER NTCLE300E3	OLD 12NC CODE 2381 645
3	3977	302SB	20302
5	3977	502SB	20502
10	3977	103SB	20103

DIMENSIONS in millimeters

Component outline for NTCLE201E3...



Component outline for NTCLE300E3...



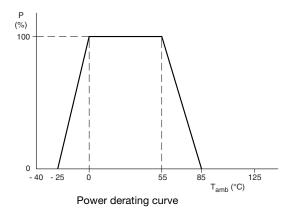
Document Number: 29051 Revision: 16-May-11 For technical questions, contact: nlr@vishay.com

Vishay BCcomponents

NTC Thermistors, 2-Point Mini Chip Sensor, Flexible Leads



DERATING



Note

Zero power is considered as measuring power max. 1 % of max. power

RESIST/	ANCE VALU	ES AT INTE	RMEDIAT	E TEMPERATURES		
					R ₂₅ -VALUE (kΩ)	
T _{OPER} (°C)	R _T /R ₂₅	<u>∆</u> T (K)	TCR (%/K)	NTCLE	201E3SB OR NTCLE300	E3SB
(0)		(K)	(70/K)	302	502	103
- 40	33.21	0.68	6.57	99.63	166.1	332.1
- 35	23.99	0.66	6.36	71.97	120.0	239.9
- 30	17.52	0.64	6.15	52.56	87.60	175.2
- 25	12.93	0.62	5.95	38.79	64.65	129.3
- 20	9.636	0.59	5.76	28.91	48.18	96.36
- 15	7.250	0.57	5.58	21.75	36.25	72.50
- 10	5.505	0.55	5.40	16.51	27.52	55.05
- 5	4.216	0.52	5.24	12.65	21.08	42.16
0	3.255	0.50	5.08	9.766	16.28	32.56
5	2.534	0.50	4.92	7.602	12.67	25.34
10	1.987	0.50	4.78	5.962	9.936	19.87
15	1.570	0.50	4.64	4.710	7.849	15.70
20	1.249	0.50	4.50	3.746	6.244	12.49
25	1.000	0.50	4.37	3.000	5.000	10.00
30	0.8059	0.50	4.25	2.418	4.030	8.059
35	0.6535	0.50	4.13	1.960	3.267	6.535
40	0.5330	0.50	4.02	1.599	2.665	5.330
45	0.4372	0.50	3.91	1.312	2.186	4.372
50	0.3605	0.50	3.80	1.082	1.803	3.606
55	0.2989	0.55	3.70	0.8966	1.494	2.989
60	0.2490	0.61	3.60	0.7470	1.245	2.490
65	0.2084	0.66	3.51	0.6253	1.042	2.084
70	0.1753	0.72	3.42	0.5259	0.8765	1.753
75	0.1481	0.77	3.33	0.4443	0.7405	1.481
80	0.1256	0.83	3.25	0.3769	0.6282	1.256
85	0.1070	0.89	3.16	0.3211	0.5352	1.070
90	0.09154	0.95	3.09	0.2746	0.4577	0.9154
95	0.07860	1.02	3.01	0.2358	0.3930	0.7860
100	0.06773	1.08	2.94	0.2032	0.3387	0.6773
105	0.05858	1.14	2.87	0.1757	0.2929	0.5858
110	0.05083	1.21	2.80	0.1525	0.2542	0.5083
115	0.04426	1.27	2.73	0.1328	0.2213	0.4426
120	0.03866	1.34	2.67	0.1160	0.1933	0.3866
125	0.03387	1.41	2.61	0.1016	0.1694	0.3387



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Vishay

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Revision: 02-Oct-12 Document Number: 91000





OPA341 OPA2341

SBOS202A - AUGUST 2001

SINGLE-SUPPLY, RAIL-TO-RAIL OPERATIONAL AMPLIFIER WITH SHUTDOWN *microAmplifier*™ Series

FEATURES

- RAIL-TO-RAIL INPUT AND OUTPUT SWING
- MicroSIZE PACKAGES
 BANDWIDTH: 5.5MHz
- SLEW RATE: 6V/μs
- QUIESCENT CURRENT: 750µA/Chan
- POWER SHUTDOWN MODE

DESCRIPTION

The OPA341 series rail-to-rail CMOS operational amplifiers are designed for low-cost, miniature applications. They are optimized for low-voltage, single-supply operation. Rail-to-rail input and output and high-speed operation make them ideal for driving sampling Analog-to-Digital (A/D) converters.

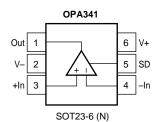
The power-saving shutdown feature makes the OPA341 ideal for portable low-power applications. The OPA341 series is also well suited for general-purpose and audio applications as well as providing I/V conversion at the output of Digital-to-Analog (D/A) converters. Single and dual versions have identical specifications for design flexibility.

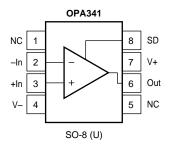
APPLICATIONS

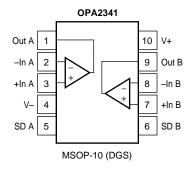
- SENSOR BIASING
- SIGNAL CONDITIONING
- DATA ACQUISITION
- PROCESS CONTROL
- ACTIVE FILTERS
- TEST EQUIPMENT

The OPA341 series operate on a single supply as low as 2.5V, and input common-mode voltage range extends 300mV beyond the supply rails. Output voltage swings to within 1mV of the supply rails with a $100k\Omega$ load. The OPA341 series offers excellent dynamic response (BW = 5.5MHz, SR = $6V/\mu s$) with a quiescent current of only $750\mu A$. The dual design features completely independent circuitry for lowest crosstalk and freedom from interaction.

The single (OPA341) packages are the tiny SOT23-6 surface mount and SO-8 surface mount. The dual (OPA2341) comes in the miniature MSOP-10 surface mount. All are specified from -55° C to $+125^{\circ}$ C and operate from -55° C to $+150^{\circ}$ C. The OPA343 provides similar performance without shutdown capability.









Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



ABSOLUTE MAXIMUM RATINGS(1)

Supply Voltage, V+ to V	6.0V
Input Voltage Range ⁽²⁾ (\	/-) - 0.5V to (V+) + 0.5V
Input Terminal ⁽³⁾	10mA
Output Short Circuit(3)	Continuous
Operating Temperature	55°C to +150°C
Storage Temperature	65°C to +150°C
Junction Temperature	150°C
Lead Temperature (soldering, 10s)	300°C

NOTES: (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. (2) Input terminals are diode-clamped to the power supply rails. Input signals that can swing more than 0.5V beyond the supply rails should be current-limited to 10mA or less. (3) Short-circuit to ground, one amplifier per package.

ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

PRODUCT	PACKAGE	PACKAGE DRAWING NUMBER	PACKAGE DESIGNATOR	SPECIFIED TEMPERATURE RANGE	PACKAGE MARKING	ORDERING NUMBER ⁽¹⁾	TRANSPORT MEDIA
OPA341NA	SOT23-6	332 "	_	–55°C to +125°C "	B41 "	OPA341NA/250 OPA341NA/3K	Tape and Reel Tape and Reel
OPA341UA "	SO-8	182 "	_ _	–55°C to +125°C	OPA341UA "	OPA341UA OPA341UA/2K5	Rails Tape and Reel
OPA2341DGSA "	MSOP-10	4073272 "	DGS "	–55°C to +125°C	C41	OPA2341DGSA/250 OPA2341DGSA/2K5	Tape and Reel Tape and Reel

NOTE: (1) Models with a slash (/) are available only in Tape and Reel in the quantities indicated (e.g., /3K indicates 3000 devices per reel). Ordering 3000 pieces of "OPA341NA/3K" will get a single 3000-piece Tape and Reel..



ELECTRICAL CHARACTERISTICS: $V_S = 2.7V$ to 5.5V

Boldface limits apply over the specified temperature range, $T_A = -55^{\circ}C$ to +125°C.

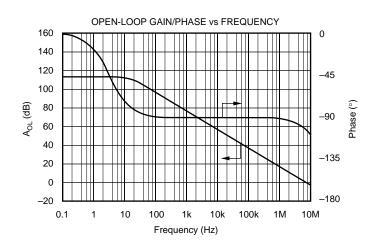
At T_A = +25°C, R_L = 10k Ω connected to $V_S/2$ and V_{OUT} = $V_S/2$, V_{ENABLE} = V_{DD} , unless otherwise noted.

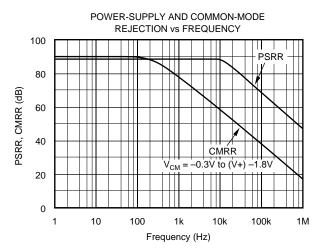
				PA341NA, UA PA2341DGSA		
PARAMETER		CONDITION	MIN	TYP	MAX	UNITS
OFFSET VOLTAGE Input Offset Voltage Drift vs Power Supply Over Temperature Channel Separation, dc	V _{OS} dV _{OS} /dT PSRR	$V_{S} = 5V$ $V_{S} = 2.7V \text{ to } 5.5V, V_{CM} = 0V$ $V_{S} = 2.7V \text{ to } 5.5V, V_{CM} = 0V$		±2 ± 2 40	±6 200 200	mV μ V/°C μV/V μ V/V μV/V
INPUT BIAS CURRENT Input Bias Current Over Temperature Input Offset Current	I _B			±0.6 ±0.2	±10 2000 ±10	pA pA pA
NOISE Input Voltage Noise, $f = 0.1Hz$ to 50 Input Voltage Noise Density, $f = 1k$ Input Current Noise Density, $f = 1k$	Hz e _n			8 25 3		μVrms nV/√Hz fA/√Hz
INPUT VOLTAGE RANGE Common-Mode Voltage Range Common-Mode Rejection Ratio Over Temperature Over Temperature	V _{CM} CMRR	$\begin{split} & V_S = 5V, \; (V-) - 0.3V < V_{CM} < (V+) - 1.8V \\ & V_S = 5V, \; (V-) - 0.1V < V_{CM} < (V+) - 1.8V \\ & V_S = 5V, \; (V-) - 0.3V < V_{CM} < (V+) + 0.3V \\ & V_S = 5V, \; (V-) - 0.1V < V_{CM} < (V+) + 0.1V \\ & V_S = 2.7V, \; (V-) - 0.3V < V_{CM} < (V+) + 0.3V \\ \end{split}$	(V-) - 0.3 (V-) - 0.1 76 74 60 58 57	90 74 70	(V+) + 0.3 (V+) + 0.1	V V dB dB dB dB
Over Temperature INPUT IMPEDANCE		$V_S = 2.7V$, $(V-) - 0.1V < V_{CM} < (V+) + 0.1V$	55			dB
Differential Common-Mode				10 ¹³ 3 10 ¹³ 6		$\Omega \mid\mid$ pF $\Omega \mid\mid$ pF
OPEN-LOOP GAIN Open-Loop Voltage Gain Over Temperature Over Temperature	A _{OL}	$\begin{aligned} R_{L} &= 100 k \Omega, \ (V-) + 5 m V < V_{O} < (V+) - 5 m V \\ R_{L} &= 100 k \Omega, \ (V-) + 5 m V < V_{O} < (V+) - 5 m V \\ R_{L} &= 2 k \Omega, \ (V-) + 200 m V < V_{O} < (V+) - 200 m V \\ R_{L} &= 2 k \Omega, \ (V-) + 200 m V < V_{O} < (V+) - 200 m V \end{aligned}$	100 100 96 94	120 110		dB dB dB dB
FREQUENCY RESPONSE Gain-Bandwidth Product Slew Rate Settling Time, 0.1% 0.01% Overload Recovery Time Total Harmonic Distortion + Noise	GBW SR t _S	$V_S = 5V$ $G = +1, C_L = 100pF$ $V_S = 5V, 2V \text{ Step, } G = +1, C_L = 100pF$ $V_S = 5V, 2V \text{ Step, } G = +1, C_L = 100pF$ $V_{IN} \bullet \text{ Gain } \leq V_S$ $V_S = 5V, V_O = 3Vp \cdot p^{(1)}, G = +1, f = 1kHz$		5.5 6 1 1.6 0.2 0.0007		MHz V/μs μs μs μs
OUTPUT Voltage Output Swing from Rail Over Temperature Over Temperature Short-Circuit Current Capacitive Load Drive	I _{SC} C _{LOAD}	$\begin{split} R_L &= 100k\Omega,\ A_{OL} > 100dB \\ R_L &= 100k\Omega,\ A_{OL} > 100dB \\ R_L &= 2k\Omega,\ A_{OL} > 96dB \\ R_L &= 2k\Omega,\ A_{OL} > 94dB \end{split}$	See Ty	1 40 ±50	5 5 200 200 eristics	mV mV mV mV
SHUTDOWN toff ton VL (Shutdown) VH (Amplifier is Active) IQSD			V- (V-) + 2	1 3	(V-) + 0.8 V+	μs μs V V nA
POWER SUPPLY Specified Voltage Range Operating Voltage Range Quiescent Current (per amplifier) Over Temperature	V _s	I _O = 0, V _S = 5V	2.7	2.5 to 5.5 0.75	5.5 1.0 1.2	V V mA mA
TEMPERATURE RANGE Specified Range Operating Range Storage Range Thermal Resistance SOT-23-6 Surface Mount MSOP-10 Surface Mount SO-8 Surface Mount	$ heta_{\sf JA}$		-55 -55 -65	200 150 150	125 150 150	°C/W °C/W °C/W °C/W °C/W

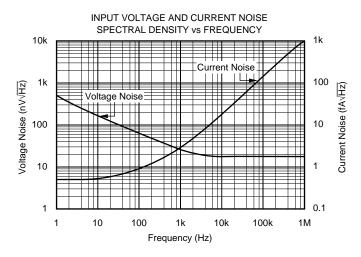
NOTE: (1) $V_{OUT} = 0.25V$ to 3.25V.

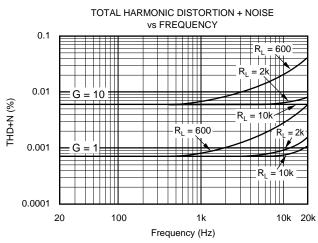


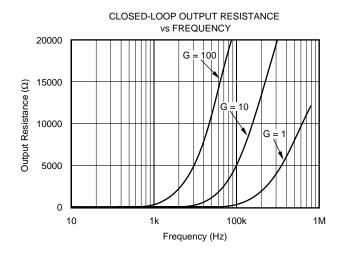
TYPICAL CHARACTERISTICS

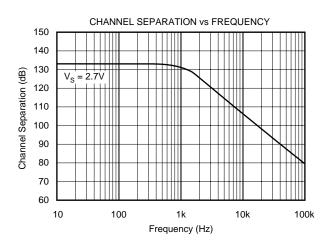


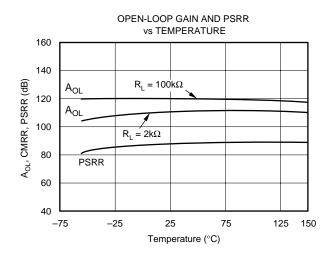


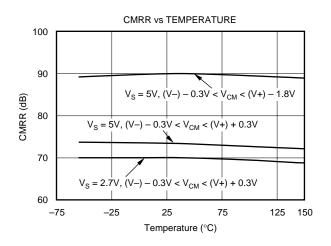


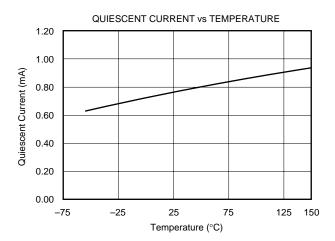


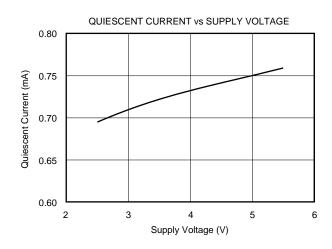


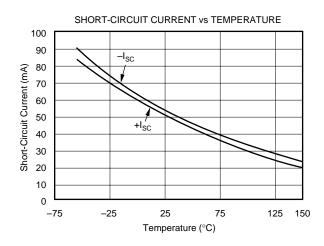


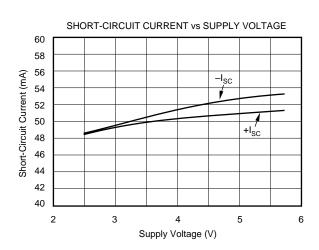


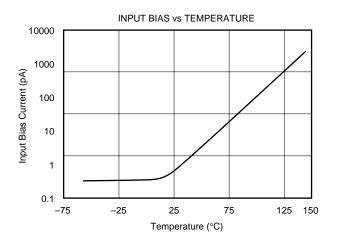


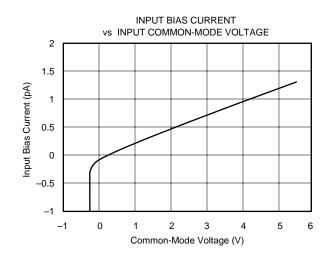


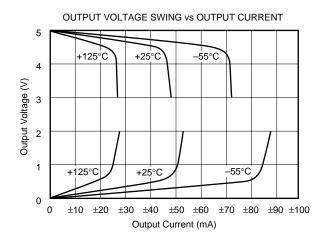


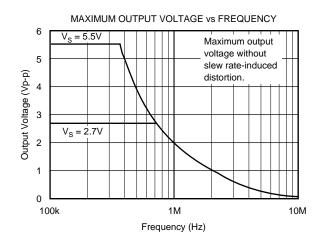


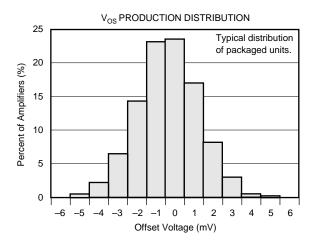


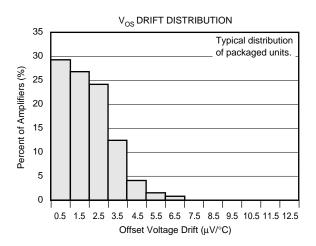




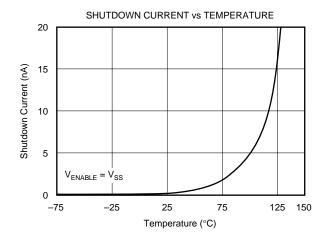


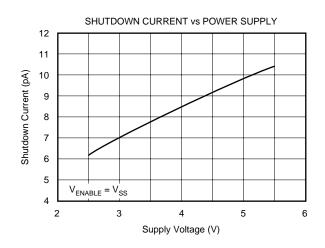


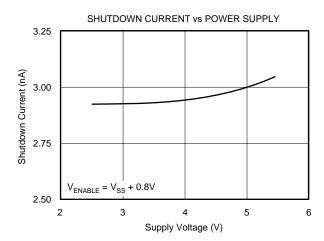


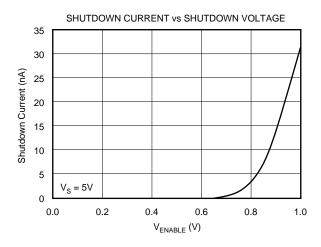


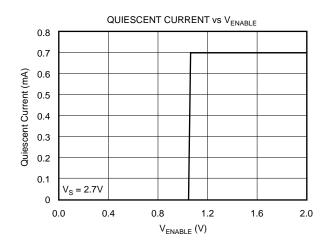


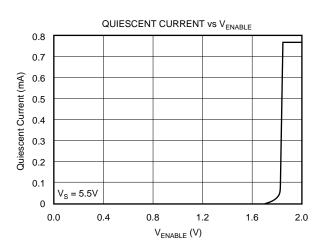




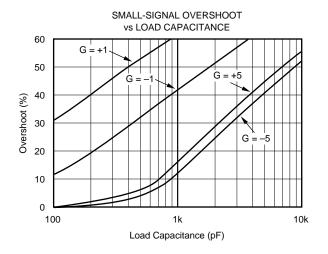


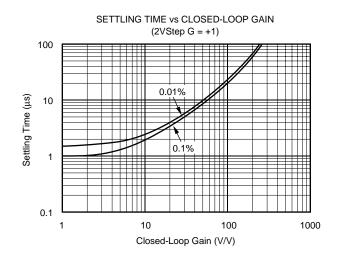


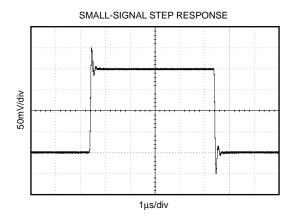


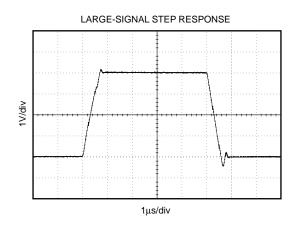


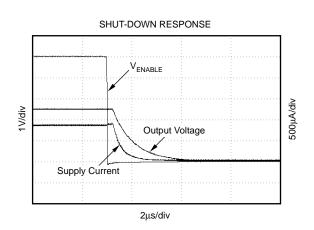


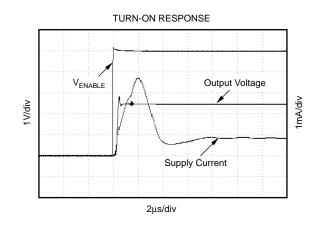












APPLICATIONS INFORMATION

OPA341 series op amps are fabricated on a state-of-the-art 0.6-micron CMOS process. They are unity-gain stable and suitable for a wide range of general-purpose applications.

Rail-to-rail I/O make them ideal for driving sampling A/D converters. In addition, excellent ac performance makes them well suited for audio applications. The class AB output stage is capable of driving 600Ω loads connected to any point between V+ and ground. Rail-to-rail input and output swing significantly increases dynamic range, especially in low-supply applications. Figure 1 shows the input and output waveforms for the OPA341 in unity-gain configuration. Operation is from a single +5V supply with a $10k\Omega$ load connected to $V_{\rm S}/2$. The input is a 5Vp-p sinusoid. Output voltage is approximately 4.98Vp-p. Power-supply pins should be bypassed with $0.01\mu F$ ceramic capacitors.

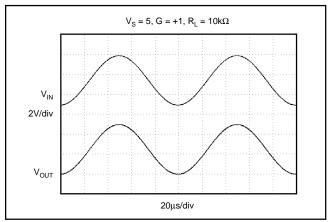


FIGURE 1. Rail-to-Rail Input and Output.

OPERATING VOLTAGE

OPA341 series op amps are fully specified from +2.7V to +5.5V. However, supply voltage may range from +2.5V to +5.5V. Parameters are tested over the specified supply range—a unique feature of the OPA341 series. In addition, many specifications apply from -55°C to +125°C. Most behavior remains virtually unchanged throughout the full operating voltage range. Parameters that vary significantly with operating voltages or temperature are shown in the Typical Characteristics.

RAIL-TO-RAIL INPUT

The input common-mode voltage range of the OPA341 series extends 300mV beyond the supply rails. This is achieved with a complementary input stage—an N-channel input differential pair in parallel with a P-channel differential pair, as shown in Figure 2. The N-channel pair is active for input voltages close to the positive rail, typically (V+) - 1.3V to 300mV above the positive supply. The P-channel pair is on for inputs from 300mV below the negative supply to approximately (V+) - 1.3V.

There is a small transition region, typically (V+) - 1.5V to (V+) - 1.1V, in which both input pairs are on. This 400mV transition region can vary ± 300 mV with process variation. Thus, the transition region (both stages on) can range from (V+) - 1.8V to (V+) - 1.4V on the low end, up to (V+) - 1.2V to (V+) - 0.8V on the high end. Within the 400mV transition region PSRR, CMRR, offset voltage, offset drift, and THD may be degraded compared to operation outside this region.

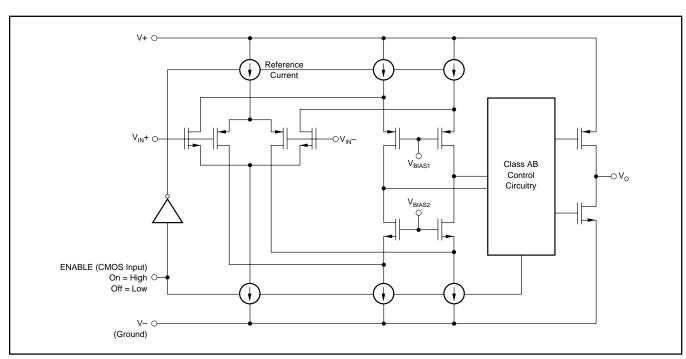


FIGURE 2. Simplified Schematic.



A double-folded cascode adds the signal from the two input pairs and presents a differential signal to the class AB output stage. Normally, input bias current is approximately 600fA, however, input voltages exceeding the power supplies by more than 300mV can cause excessive current to flow in or out of the input pins. Momentary voltages greater than 300mV beyond the power supply can be tolerated if the current on the input pins is limited to 10mA. This is easily accomplished with an input resistor, as shown in Figure 3. Many input signals are inherently current-limited to less than 10mA, therefore, a limiting resistor is not required.

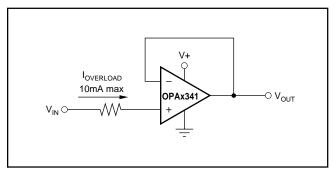


FIGURE 3. Input Current Protection for Voltages Exceeding the Supply Voltage.

RAIL-TO-RAIL OUTPUT

A class AB output stage with common-source transistors is used to achieve rail-to-rail output. For light resistive loads (> $50k\Omega$), the output voltage is typically a few millivolts from the supply rails. With moderate resistive loads ($2k\Omega$ to $50k\Omega$), the output can swing to within a few tens of millivolts from the supply rails and maintain high open-loop gain. See the typical characteristic "Output Voltage Swing vs Output Current."

CAPACITIVE LOAD AND STABILITY

OPA341 series op amps can drive a wide range of capacitive loads. However, all op amps under certain conditions may become unstable. Op amp configurations, gain, and load value are just a few of the factors to consider when determining stability. An op amp in unity-gain configuration is the most susceptible to the effects of capacitive load. The

capacitive load reacts with the op amp's output resistance, along with any additional load resistance, to create a pole in the small-signal response which degrades the phase margin. In unity gain, OPA341 series op amps perform well, with a pure capacitive load up to approximately 1000pF. Increasing gain enhances the amplifier's ability to drive more capacitance. See the typical characteristic "Small-Signal Overshoot vs Capacitive Load."

One method of improving capacitive load drive in the unitygain configuration is to insert a 10Ω to 20Ω resistor in series with the output, as shown in Figure 4. This significantly reduces ringing with large capacitive loads. However, if there is a resistive load in parallel with the capacitive load, R_S creates a voltage divider. This introduces a DC error at the output and slightly reduces output swing. This error may be insignificant. For instance, with $R_L=10 k\Omega$ and $R_S=20\Omega$, there is only about a 0.2% error at the output.

DRIVING A/D CONVERTERS

OPA341 series op amps are optimized for driving medium speed (up to 100kHz) sampling A/D converters. However, they also offer excellent performance for higher-speed converters. The OPA341 series provides an effective means of buffering the A/D converter's input capacitance and resulting charge injection while providing signal gain. For applications requiring high accuracy, the OPA340 series is recommended.

The OPA341 implements a power-saving shutdown feature particularly useful for low-power sampling applications. Figure 5 shows the OPA341 driving the ADS7816, a 12-bit micro-power sampling converter available in the tiny MSOP-8 package. With the OPA341 in non-inverting configuration, an RC network at the amplifier's output is used as an anti-aliasing filter. By tying the enable of the OPA341 to the shutdown of the ADS7816, additional power-savings can be used for sampling applications. To effectively drive the ADS7816, timing delay was introduced between the two devices, see Figure 5. Alternative applications may need additional timing adjustments.

Figure 6 shows the OPA341 configured as a speech bandpass filter. Figure 7 shows the OPA341 configured as a transimpedance amplifier.

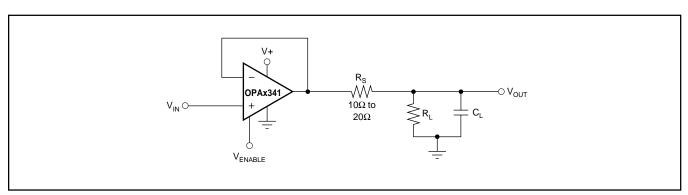


FIGURE 4. Series Resistor in Unity-Gain Configuration Improves Capacitive Load Drive.



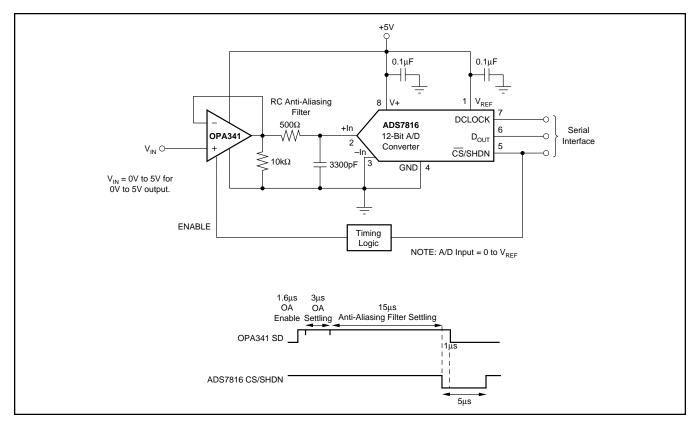


FIGURE 5. OPA341 in Noninverting Configuration Driving the ADS7816 with Timing Diagram.

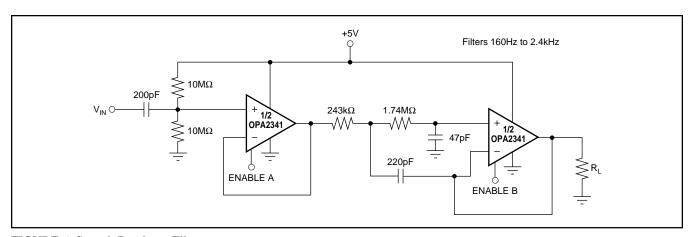


FIGURE 6. Speech Bandpass Filter.

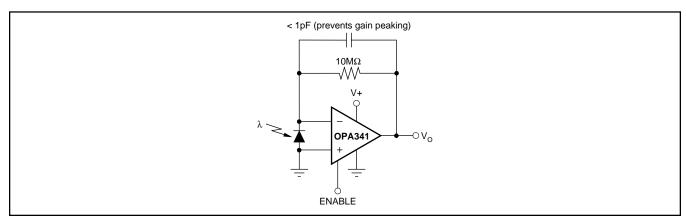


FIGURE 7. Transimpedance Amplifier.







10-Jun-2014

PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package	Pins	Package	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
	(1)		Drawing		Qty	(2)	(6)	(3)		(4/5)	
OPA2341DGSA/250	ACTIVE	VSSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-2-260C-1 YEAR	-55 to 125	C41	Samples
OPA2341DGSA/250G4	ACTIVE	VSSOP	DGS	10	250	Green (RoHS & no Sb/Br)	CU NIPDAUAG	Level-2-260C-1 YEAR	-55 to 125	C41	Samples
OPA341NA/250	ACTIVE	SOT-23	DBV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-55 to 125	B41	Samples
OPA341NA/250G4	ACTIVE	SOT-23	DBV	6	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-55 to 125	B41	Samples
OPA341NA/3K	ACTIVE	SOT-23	DBV	6	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-55 to 125	B41	Samples
OPA341UA	ACTIVE	SOIC	D	8	75	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	-55 to 125	OPA 341UA	Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check http://www.ti.com/productcontent for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

Pb-Free (RoHS): TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes. **Pb-Free** (RoHS Exempt): This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

Green (RoHS & no Sb/Br): TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.



PACKAGE OPTION ADDENDUM

10-Jun-2014

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

www.ti.com 26-Jan-2013

TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
В0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

Device	Package Type	Package Drawing			Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA2341DGSA/250	VSSOP	DGS	10	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1

PACKAGE MATERIALS INFORMATION

www.ti.com 26-Jan-2013



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA2341DGSA/250	VSSOP	DGS	10	250	210.0	185.0	35.0

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ADC0801, ADC0802, ADC0803, ADC0804, ADC0805

SNOSBI1C -NOVEMBER 2009-REVISED JUNE 2015

ADC080x 8-Bit, µP-Compatible, Analog-to-Digital Converters

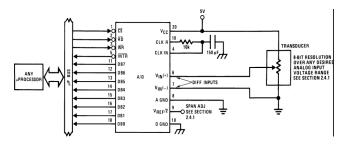
Features

- Compatible With 8080-µP Derivatives No Interfacing Logic Needed - Access Time 135 ns
- Easy Interface to All Microprocessors, or Operates as a Stand-Alone Deivce
- Differential Analog Voltage Inputs
- Logic Inputs and Outputs Meet Both MOS and TTL Voltage-Level Specifications
- Works With 2.5-V (LM336) Voltage Reference
- On-Chip Clock Generator
- 0-V to 5-V Analog Input Voltage Range With Single 5-V Supply
- No Zero Adjust Required
- 0.3-Inch Standard Width 20-Pin DIP Package
- 20-Pin Molded Chip Carrier or Small Outline Package
- Operates Ratiometrically or With 5 V_{DC}, 2.5 V_{DC}, or Analog Span Adjusted Voltage Reference
- **Key Specifications**
 - Resolution: 8 Bits
 - Total Error: ±1/4 LSB, ±1/2 LSB and ±1 LSB
 - Conversion Time: 100 µs

2 Applications

- Operates With Any 8-Bit µP Processors or as a Stand-Alone Device
- Interface to Temp Sensors, Voltage Sources, and Transducers

Typical Application Schematic



3 Description

The ADC0801, ADC0802, ADC0803, ADC0804, and ADC0805 devices are CMOS 8-bit successive approximation converters (ADC) that use a differential potentiometric ladder — similar to the 256R products. These converters are designed to allow operation with the NSC800 and INS8080A derivative control bus with Tri-state output latches directly driving the data bus. These ADCs appear like memory locations or I/O ports to the microprocessor and no interfacing logic is needed.

Differential analog voltage inputs allow increasing the common-mode rejection and offsetting the analog zero input voltage value. In addition, the voltage reference input can be adjusted to allow encoding any smaller analog voltage span to the full 8 bits of resolution.

Device Information⁽¹⁾

PART NUMBER	PACKAGE	BODY SIZE (NOM)
ADC0801, ADC0803	PDIP (20)	26.073 mm × 6.604 mm
ADC0802,	PDIP (20)	26.073 mm × 6.604 mm
ADC0804	SOIC (20)	12.80 mm × 7.50 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.

ADC0801 Specified With ±1/4 LSB Accuracy

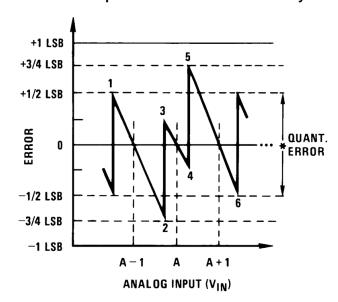




Table of Contents	T	abl	le	of	Contents
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Features 1		8.2 Functional Block Diagram	12
Applications 1		8.3 Feature Description	12
Description 1		8.4 Device Functional Modes	14
	9	Application and Implementation	18
•		9.2 Typical Applications	2
G	10	Power Supply Recommendations	48
•	11	Layout	48
6.4 Thermal Information		11.1 Layout Guidelines	48
6.5 Operating Ratings 5	12	Device and Documentation Support	49
6.6 Electrical Characteristics		12.1 Related Links	49
6.7 AC Electrical Characteristics 5		12.2 Community Resources	49
6.8 Typical Characteristics		12.3 Trademarks	49
Parameter Measurement Information		12.4 Electrostatic Discharge Caution	49
7.1 Tri-State Test Circuits and Waveforms		12.5 Glossary	49
Detailed Description 11	13	Mechanical, Packaging, and Orderable Information	49
	6.4 Thermal Information 4 6.5 Operating Ratings 5 6.6 Electrical Characteristics 5 6.7 AC Electrical Characteristics 5 6.8 Typical Characteristics 8 Parameter Measurement Information 10	Applications 1 Description 1 Revision History 2 Pin Configuration and Functions 3 Specifications 4 6.1 Absolute Maximum Ratings 4 6.2 ESD Ratings 4 6.3 Recommended Operating Conditions 4 6.4 Thermal Information 4 6.5 Operating Ratings 5 6.6 Electrical Characteristics 5 6.7 AC Electrical Characteristics 5 6.8 Typical Characteristics 8 Parameter Measurement Information 10 7.1 Tri-State Test Circuits and Waveforms 10 Detailed Description 11 13	Applications 1 8.3 Feature Description 8.4 Device Functional Modes 9 Application and Implementation 9.1 Application and Implementation 9.1 Application Information 9.2 Typical Applications 9.2 Typical Applications 9.3 System Examples 9.3 System Ex

4 Revision History

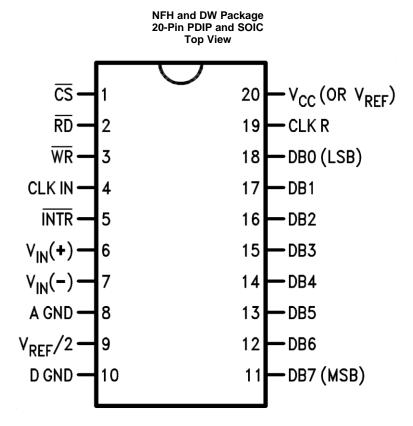
Changes from Revision B (Feburary 2013) to Revision C

Page

Added Pin Configuration and Functions section, ESD Ratings table, Feature Description section, Device Functional
Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device
and Documentation Support section, and Mechanical, Packaging, and Orderable Information section



5 Pin Configuration and Functions



Pin Functions

	PIN		
NO.	NAME	I/O	DESCRIPTION
1	CS	I	Chip Select
2	RD	I	Read
3	WR	I	Write
4	CLK IN	I	External Clock input or use internal clock gen with external RC elements
5	INTR	0	Interrupt request
6	V _{IN} (+)	1	Differential analog input+
7	V _{IN} (–)	I	Differential analog input-
8	A GND	I	Analog ground pin
9	V _{REF} /2	1	Reference voltage input for adjustment to correct full scale reading
10	D GND	1	Digital ground pin
11	DB7	0	Data bit 7
12	DB6	0	Data bit 6
13	DB5	0	Data bit 5
14	DB4	0	Data bit 4
15	DB3	0	Data bit 3
16	DB2	0	Data bit 2
17	DB1	0	Data bit 1
18	DB0 (LSB)	0	Data bit 0
19	CLK R	I	RC timing resistor input pin for internal clock gen
20	V _{CC} (or V _{REF})	I	+5V supply voltage, also upper reference input to the ladder



6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted) (1)(2)

		MIN	MAX	UNIT	
Supply voltage (V _{CC}) ⁽³			6.5	V	
Voltage	Logic control inputs	-0.3	18	V	
	At other input and outputs	-0.3	$(V_{CC} + 0.3)$	V	
	Dual-In-Line Package (plastic		260		
Lead Temperature	Dual-In-Line Package (ceramic)		300		
(Soldering, 10 seconds)	Surface Mount Package Vapor Phase (60 seconds)		215	°C	
,	Infrared (15 seconds)		220		
Storage Temperature		-65	150		
Package Dissipation a	$t T_A = 25^{\circ}C$		875	mW	

⁽¹⁾ Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001 (1)	±800	V

⁽¹⁾ JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

	MIN	NOM	MAX	UNIT
VCC	4.5	5	5.5	V
Analog Input Voltage	GND - 0.05		$V_{CC} + 0.05$	V_{DC}

6.4 Thermal Information

	TUEDMAL METDIO(1)		ADC0802, ADC0804	
	THERMAL METRIC ⁽¹⁾	NFH (PDIP)	DW (SOIC)	UNIT
		20 PINS	20 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	38.5	63.8	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	23.4	27.2	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	19.5	31.8	°C/W
Ψ_{JT}	Junction-to-top characterization parameter	8.7	5.7	°C/W
Ψ_{JB}	Junction-to-board characterization parameter	19.4	31.3	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	_	_	°C/W

For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report, SPRA953.

Submit Documentation Feedback

⁽²⁾ If Military/Aerospace specified devices are required, contact the Sales Office/Distributors for availability and specifications.

⁽³⁾ A Zener diode exists, internally, from V_{CC} to GND and has a typical breakdown voltage of 7 V_{DC}.



6.5 Operating Ratings

over operating free-air temperature range (unless otherwise noted)(1)(2).

		MIN	MAX	UNIT
Temperature	ADC0804LCJ	-40	85	
	ADC0801/02/03/05LCN	-40	85	°C
	ADC0804LCN	0	70	
	ADC0802/04LCWM	0	70	
Range of V _{CC}		4.5	6.3	V_{DC}

⁽¹⁾ Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. DC and AC electrical specifications do not apply when operating the device beyond its specified operating conditions.

6.6 Electrical Characteristics

The following specifications apply for $V_{CC} = 5 V_{DC}$, $T_{MIN} \le T_A \le T_{MAX}$ and $f_{CLK} = 640$ kHz (unless otherwise specified).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
ADC0801: Total Adjusted Error ⁽¹⁾	With Full-Scale Adj. (See Full-Scale)			±1/4	
ADC0802: Total Unadjusted Error ⁽¹⁾	V _{REF} /2=2.500 V _{DC}			±1/2	
ADC0803: Total Adjusted Error ⁽¹⁾	With Full-Scale Adj. (See Full-Scale)			±1/2	LSB
ADC0804: Total Unadjusted Error	V _{REF} /2=2.500 VDC			±1	LOD
ADC0805: Total Unadjusted Error	V _{REF} /2-No Connection			±1	
V /O lamest Designation of (Pin O)	ADC0801/02/03/05	2.5	8		1.0
V _{REF} /2 Input Resistance (Pin 9)	ADC0804 (2)	0.75	1.1		kΩ
Analog Input Voltage Range	V(+) or V(-) ⁽³⁾	GND-0.05		V _{CC} +0.05	V_{DC}
DC Common-Mode Error	Over Analog Input Voltage Range		±1/16	±1/8	LSB
Power Supply Sensitivity	$\rm V_{CC} = 5~\rm V_{DC}~\pm 10\%~Over~Allowed~\rm V_{IN}(+)~and~\rm V_{IN}(-)~\rm Voltage~Range^{(3)}$		±1/16	±1/8	LSB

⁽¹⁾ None of these ADCs requires a zero adjust (see *Zero Error*). To obtain zero code at other analog input voltages see *Errors and Reference Voltage Adjustments*.

6.7 AC Electrical Characteristics

The following specifications apply for $V_{CC}=5$ V_{DC} and $T_{MIN} \le T_A \le T_{MAX}$ (unless otherwise specified)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
T _C	Conversion Time	$f_{CLK} = 640 \text{ kHz}^{(1)}$	103		114	μs
		See (2)(1)	66		73	1/fCLK
,	Clock Frequency	$V_{CC} = 5V^{(2)}$	100	640	1460	kHz
f _{CLK}	Clock Duty Cycle	V _{CC} = 5V (-)	40%		60%	
CR	Conversion Rate in Free-Running Mode	INTR tied to $\overline{\text{WR}}$ with $\overline{\text{CS}} = 0$ VDC, $f_{\text{CLK}} = 640 \text{ kHz}$	8770		9708	conv/s

⁽¹⁾ Accuracy is specified at f_{CLK} = 640 kHz. At higher clock frequencies accuracy can degrade. For lower clock frequencies, the duty cycle limits can be extended so long as the minimum clock high time interval or minimum clock low time interval is no less than 275 ns.

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⁽²⁾ All voltages are measured with respect to GND, unless otherwise specified. The separate A GND point should always be wired to the D GND.

⁽²⁾ The V_{REF}/2 pin is the center point of a two-resistor divider connected from V_{CC} to ground. In all versions of the ADC0801, ADC0802, ADC0803, and ADC0805, and in the ADC0804LCJ, each resistor is typically 16 kΩ. In all versions of the ADC0804 except the ADC0804LCJ, each resistor is typically 2.2 kΩ.

⁽³⁾ For V_{IN}(−)≥ VIN(+) the digital output code will be 0000 0000. Two on-chip diodes are tied to each analog input (see block diagram) which will forward conduct for analog input voltages one diode drop below ground or one diode drop greater than the V_{CC} supply. Be careful, during testing at low V_{CC} levels (4.5V), as high level analog inputs (5V) can cause this input diode to conduct–especially at elevated temperatures, and cause errors for analog inputs near full-scale. The spec allows 50 mV forward bias of either diode. This means that as long as the analog V_{IN} does not exceed the supply voltage by more than 50 mV, the output code will be correct. To achieve an absolute 0 V_{DC} to 5 V_{DC} input voltage range will therefore require a minimum supply voltage of 4.950 V_{DC} over temperature variations, initial tolerance and loading.

⁽²⁾ With an asynchronous start pulse, up to 8 clock periods may be required before the internal clock phases are proper to start the conversion process. The start request is internally latched. Refer to *Detailed Description*.



AC Electrical Characteristics (continued)

The following specifications apply for $V_{CC}=5$ V_{DC} and $T_{MIN} \le T_A \le T_{MAX}$ (unless otherwise specified)

			TEST CONDITIONS		TVD	MAN	LINIT
	PARA	AMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
$t_{W(\overline{WR})}$	Width of WR Input	(Start Pulse Width)	$\overline{\text{CS}} = 0 \text{ VDC}^{(3)}$	100			
tACC	Access Time (Dela Output Data Valid)	y from Falling Edge of RD to	C _L = 100 pF		135	200	ne
t1H, t0H	Tri-State Control (I to Hi-Z State)	Delay from Rising Edge of RD	C _L = 10 pF, R _L = 10k (See <i>Tri-State Test Circuits and Waveforms</i>)		125	200	ns
t_{WI},t_{RI}	Delay from Falling of INTR	Edge of WR or RD to Reset			300	450	
C_{IN}	Input Capacitance	of Logic Control Inputs			5	7.5	nE.
C_{OUT}	Tri-State Output Ca	apacitance (Data Buffers)			5	7.5	pF
CONTR	ROL INPUTS [Note:	CLK IN (Pin 4) is the input of a	Schmitt trigger circuit and is therefore sp	pecified sepa	arately]		
V _{IN} (1)	Logical "1" Input Vo	oltage (Except Pin 4 CLK IN)	V _{CC} = 5.25 VDC	2		15	\/
V _{IN} (0)	Logical "0" Input Voltage (Except Pin 4 CLK IN)		V _{CC} = 4.75 VDC			8.0	V_{DC}
I _{IN} (1)	Logical "1" Input Current (All Inputs)		V _{IN} = 5 VDC		0.005	1	
I _{IN} (0)	Logical "0" Input Current (All Inputs)		V _{IN} = 0 VDC	-1	-0.005		μA_{DC}
CLOCK	IN AND CLOCK R						
V _T +	CLK IN (Pin 4) Pos	sitive Going Threshold Voltage		2.7	3.1	3.5	
V _T -	CLK IN (Pin 4) Negative Going Threshold Voltage			1.5	1.8	2.1	
V_{H}	CLK IN (Pin 4) Hys	steresis (V _T +)–(V _T –)		0.6	1.3	2	V_{DC}
V _{OUT} (0)	Logical "0" CLK R	Output Voltage	I _O = 360 μA, V _{CC} = 4.75 VDC			0.4	vDC.
V _{OUT} (1)	Logical "1" CLK R	Output Voltage	I _O = -360 μA, V _{CC} = 4.75 VDC	2.4			
DATA	OUTPUTS AND INT	·R				•	
V _{OUT}	Logical "0" Output	Data Outputs	$I_{OUT} = 1.6 \text{ mA}, V_{CC} = 4.75 V_{DC}$			0.4	
(0)	Voltage	INTR Output	$I_{OUT} = 1.0 \text{ mA}, V_{CC} = 4.75 V_{DC}$			0.4	.,
V _{OUT}	1 ' 1"4" 0 ' '	14.16	$I_{O} = -360 \mu A, V_{CC} = 4.75 V_{DC}$	2.4			V_{DC}
(1)	Logical "1" Output	Voltage	$I_{O} = -10 \mu A, V_{CC} = 4.75 V_{DC}$	4.5			
	Tri-State Disabled	Output Leakage (All Data	V _{OUT} = 0 VDC	-3			
I _{OUT}	Buffers)		V _{OUT} = 5 VDC			3	μA _{DC}
I _{SOURC}	,		V _{OUT} Short to GND, T _A = 2 5°C	4.5	6		mA _{DC}
I _{SINK}			V_{OUT} Short to V_{CC} , $T_A = 25^{\circ}C$	9	16		50
	R SUPPLY		<u></u>				
	Supply Current	ADC0801/02/03/04LCJ/05	f _{CLK} = 640 kHz, V _{REF} /2 = NC,		1.1	1.8	
I _{CC}	(Includes Ladder Current)	ADC0804LCN/LCWM	$T_A = 25^{\circ}\text{C}$ and $\overline{\text{CS}} = 5 \text{ V}$		1.9	2.5	mA

⁽³⁾ The $\overline{\text{CS}}$ input is assumed to bracket the $\overline{\text{WR}}$ strobe input and therefore timing is dependent on the $\overline{\text{WR}}$ pulse width. An arbitrarily wide pulse width will hold the converter in a reset mode and the start of conversion is initiated by the low to high transition of the $\overline{\text{WR}}$ pulse.



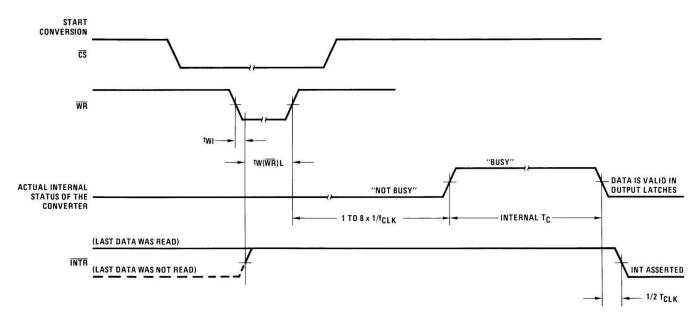
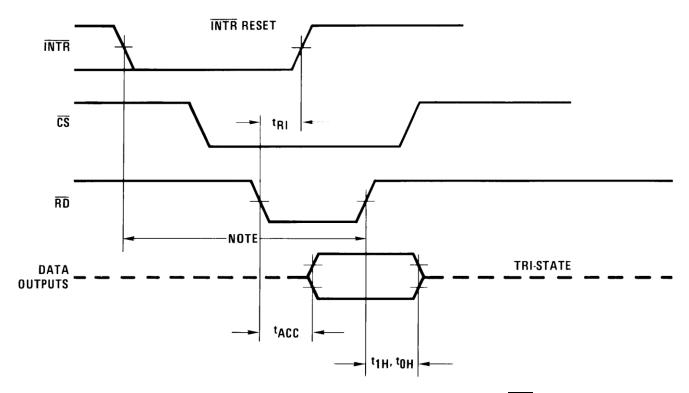


Figure 1. Start Conversion



Note: Read strobe must occur 8 clock periods ($8/f_{CLK}$) after assertion of interrupt to specify reset of \overline{INTR} .

Figure 2. Output Enable and Reset With INTR



6.8 Typical Characteristics

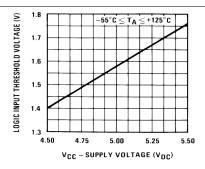


Figure 3. Logic Input Threshold Voltage vs Supply Voltage

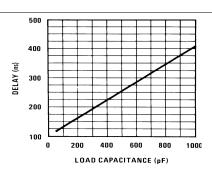


Figure 4. Delay From Falling Edge of RD to Output Data Valid vs Load Capacitance

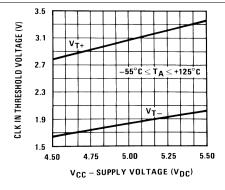


Figure 5. CLK IN Schmitt Trip Levels vs Supply Voltage

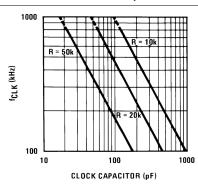


Figure 6. f_{CLK} vs Clock Capacitor

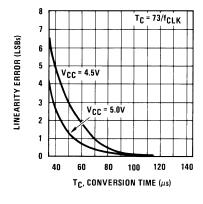


Figure 7. Full-Scale Error vs Conversion Time

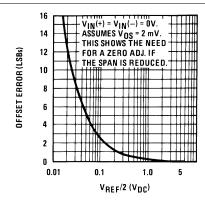
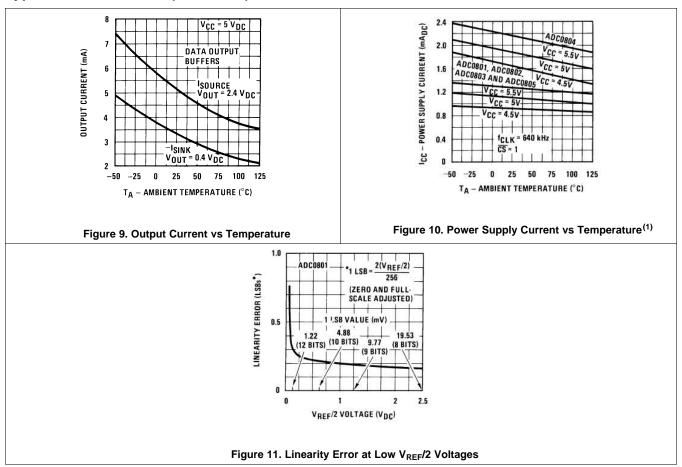


Figure 8. Effect of Unadjusted Offset Error vs V_{REF}/2 Voltage



Typical Characteristics (continued)

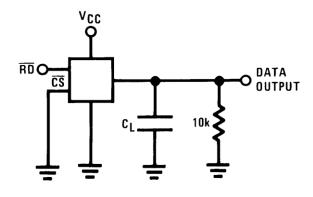


(1) The V_{REF}/2 pin is the center point of a two-resistor divider connected from V_{CC} to ground. In all versions of the ADC0801, ADC0802, ADC0803, and ADC0805, and in the ADC0804LCJ, each resistor is typically 16 kΩ. In all versions of the ADC0804 except the ADC0804LCJ, each resistor is typically 2.2 kΩ.



7 Parameter Measurement Information

7.1 Tri-State Test Circuits and Waveforms



 $C_L = 10 pF$

VCC FD F0%

GND F10%

DATA OUTPUTS

GND F10%

GND F10%

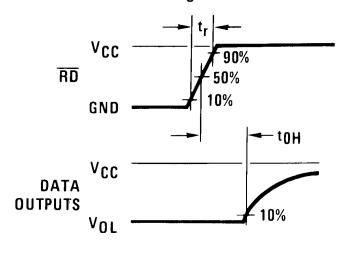
GND F11H

OUTPUTS

Figure 12. RD to Data Output Falling Edge Test Load Condition

VCC VCC DATA OUTPUT

Figure 13. RD to Data Output Falling Edge Test Timing



 $C_L = 10 pF$

Figure 14. RD to Data Output Rising Edge Test Load Condition

Figure 15. RD to Data Output Rising Edge Test Timing



8 Detailed Description

8.1 Overview

The ADC0801 series are versatile 8-Bit µP compatible general purpose ADC converters operate on single 5-V supply. These devices are treated as a memory location or I/O port to a micro-processor system without additional interface logic. The outputs are Tri-state latched which facilitate interfacing to micro-processor control bus. The converter is designed with a differential potentiometric ladder, a circuit equivalent of the 256R network. It contains analog switches sequenced by successive approximation logic. A functional diagram of the ADC converter is shown in *Functional Block Diagram*. All of the package pinouts are shown and the major logic control paths are drawn in heavier weight lines. The differential analog voltage input has good common mode-rejection and permits offsetting the analog zero-input voltage value. Moreover, the input reference voltage can be adjusted to allow encoding small analog voltage span to the full 8-bits resolution. To ensure start-up under all possible conditions, an external WR pulse is required during the first power-up cycle.

Using a SAR logic the most significant bit is tested first and after 8 comparisons (64 clock cycles) a digital 8-bit binary code (1111 1111 = full-scale) is transferred to an output latch and then an interrupt is asserted (INTR makes a high-to-low transition). A conversion in process can be interrupted by issuing a second start command. The device may be operated in the free-running mode by connecting INTR to the WR input with CS=0.

On the high-to-low transition of the $\overline{\text{WR}}$ input the internal SAR latches and the shift register stages are reset. As long as the $\overline{\text{CS}}$ input and $\overline{\text{WR}}$ input remain low, the ADC will remain in a reset state. Conversion will start from 1 to 8 clock periods after at least one of these inputs makes a low-to-high transition.

The converter is started by having $\overline{\text{CS}}$ and $\overline{\text{WR}}$ simultaneously low. This sets the start flip-flop (F/F) and the resulting "1" level resets the 8-bit shift register, resets the Interrupt (INTR) F/F and inputs a "1" to the D flop, F/F1, which is at the input end of the 8-bit shift register. Internal clock signals then transfer this "1" to the Q output of F/F1. The AND gate, G1, combines this "1" output with a clock signal to provide a reset signal to the start F/F. If the set signal is no longer present (either $\overline{\text{WR}}$ or $\overline{\text{CS}}$ is a "1") the start F/F is reset and the 8-bit shift register then can have the "1" clocked in, which starts the conversion process. If the set signal were to still be present, this reset pulse would have no effect (both outputs of the start F/F would momentarily be at a "1" level) and the 8-bit shift register would continue to be held in the reset mode. This logic therefore allows for wide $\overline{\text{CS}}$ and $\overline{\text{WR}}$ signals and the converter will start after at least one of these signals returns high and the internal clocks again provide a reset signal for the start F/F.

After the "1" is clocked through the 8-bit shift register (which completes the SAR search) it appears as the input to the D-type latch, LATCH 1. As soon as this "1" is output from the shift register, the AND gate, G2, causes the new digital word to transfer to the Tri-state output latches. When LATCH 1 is subsequently enabled, the Q output makes a high-to-low transition which causes the INTR F/F to set. An inverting buffer then supplies the INTR input signal.

Note this SET control of the INTR F/F remains low for 8 of the external clock periods (as the internal clocks run at 1/8 of the frequency of the external clock). If the data output is continuously enabled (CS and RD both held low), the INTR output will still signal the end of conversion (by a high-to-low transition), because the SET input can control the Q output of the INTR F/F even though the RESET input is constantly at a M "1M" level in this operating mode. This INTR output will therefore stay low for the duration of the SET signal, which is 8 periods of the external clock frequency (assuming the ADC is not started during this interval).

When operating in the free-running or continuous conversion mode ($\overline{\text{INTR}}$ pin tied to $\overline{\text{WR}}$ and $\overline{\text{CS}}$ wired low – see *Continuous Conversions*), the START F/F is SET by the high-to-low transition of the $\overline{\text{INTR}}$ signal. This resets the SHIFT REGISTER which causes the input to the D-type latch, LATCH 1, to go low. As the latch enable input is still present, the $\overline{\text{Q}}$ output will go high, which then allows the $\overline{\text{INTR}}$ F/F to be RESET. This reduces the width of the resulting $\overline{\text{INTR}}$ output pulse to only a few propagation delays (approximately 300 ns).

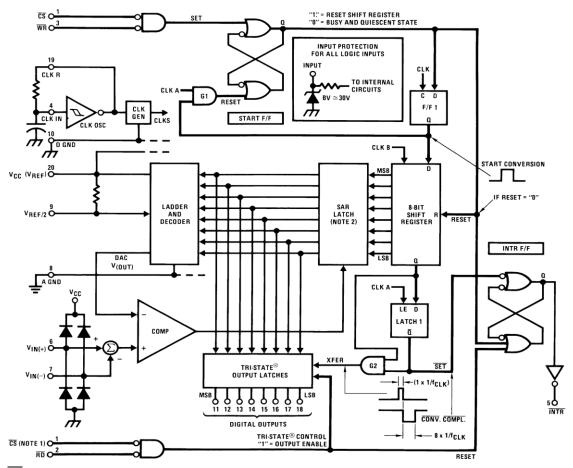
When data is to be read, the combination of both \overline{CS} and \overline{RD} being low will cause the \overline{INTR} F/F to be reset and the Tri-state output latches will be enabled to provide the 8-bit digital outputs.

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8.2 Functional Block Diagram



- (1) CS shown twice for clarity.
- (2) SAR = Successive Approximation Register.

8.3 Feature Description

8.3.1 Understanding ADC Error Specs

A perfect ADC transfer characteristic (staircase waveform) is shown in Figure 16 and Figure 17. The horizontal scale is analog input voltage and the particular points labeled are in steps of 1 LSB (19.53 mV with 2.5V tied to the VREF/2 pin). The digital output codes that correspond to these inputs are shown as D-1, D, and D+1. For the perfect ADC, not only will center- value (A-1, A, A+1,) analog inputs produce the cor- rect output digital codes, but also each riser (the transitions between adjacent output codes) will be located $\pm 1/2$ LSB away from each center-value. As shown, the risers are ideal and have no width. Correct digital output codes will be provided for a range of analog input voltages that extend $\pm 1/2$ LSB from the ideal center-values. Each tread (the range of analog input voltage that provides the same digital output code) is therefore 1 LSB wide.

Figure 19 shows a worst case error plot for the ADC0801. All center-valued inputs are guaranteed to produce the correct output codes and the adjacent risers are specified to be no closer to the center-value points than $\pm 1/4$ LSB. In other words, if we apply an analog input equal to the center-value $\pm 1/4$ LSB, we guarantee that the ADC will produce the correct digital code. The maximum range of the position of the code transition is indicated by the horizontal arrow and it is specified to be no more than 1/2 LSB.

The error curve of Figure 21 shows a worst case error plot for the ADC0802. Here we guarantee that if we apply an analog input equal to the LSB analog voltage center-value the ADC will produce the correct digital code.



Feature Description (continued)

Next to each transfer function is shown the corresponding error plot. Many people may be more familiar with error plots than transfer functions. The analog input voltage to the ADC is provided by either a linear ramp or by the discrete output steps of a high resolution DAC. Notice that the error is continuously displayed and includes the quantization uncertainty of the ADC. For example the error at point 1 of Figure 21 is +1/2 LSB because the digital code appeared 1/2 LSB in advance of the center-value of the tread. The error plots always have a constant negative slope and the abrupt up-side steps are always 1 LSB in magnitude.

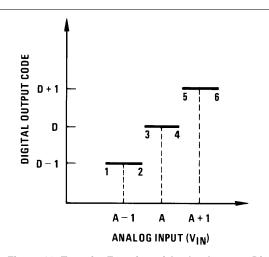


Figure 16. Transfer Function of Analog Input vs Digital Output Code in Ideal ADC

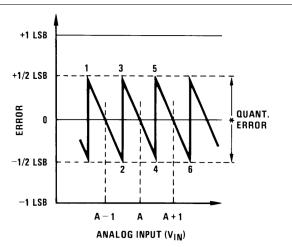


Figure 17. Clarifying the Error Specs of an ADC Converter Accuracy=±0 LSB: A Perfect ADC

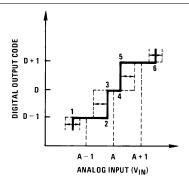


Figure 18. Transfer Function of Analog Input vs Digital Output Code for ±1/4 LSB Accuracy ADC

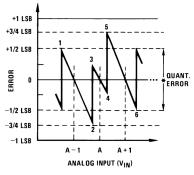


Figure 19. Clarifying the Error Specs of an ADC Converter Accuracy =±1/4 LSB

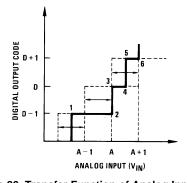


Figure 20. Transfer Function of Analog Input vs Digital Output Code for $\pm 1/2$ LSB Accuracy ADC

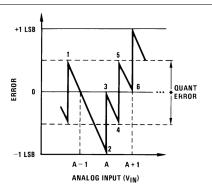


Figure 21. Clarifying the Error Specs of an ADC Converter Accuracy = ±1/2 LSB



Feature Description (continued)

8.3.2 Digital Control Inputs

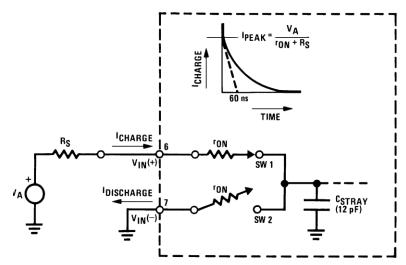
The digital control inputs $(\overline{CS}, RD, and \overline{WR})$ meet standard TLL logic voltage levels. These signals have been renamed when compared to the standard ADC Start and Output Enable labels. In addition, these inputs are active low to allow an easy interface to microprocessor control busses. For non-microprocessor based applications, the \overline{CS} input (pin 1) can be grounded and the standard ADC Start function is obtained by an active low pulse applied at the \overline{WR} input (pin 3) and the Output Enable function is caused by an active low pull at the \overline{RD} input (pin 2).

8.4 Device Functional Modes

8.4.1 Analog Input Modes

8.4.1.1 Normal Mode

Due to the internal switching action, displacement currents will flow at the analog inputs. This is due to on-chip stray capacitance to ground as shown in Figure 22.



 r_{ON} of SW 1 and SW 2.5 k Ω r= r_{ON} C_{STRAY} × 5 k Ω x 12 pF = 60 ns

Figure 22. Analog Input Impedance

The voltage on this capacitance is switched and will result in currents entering the $V_{IN}(+)$ input pin and leaving the $V_{IN}(-)$ input which will depend on the analog differential input voltage levels. These current transients occur at the leading edge of the internal clocks. They rapidly decay and do not cause errors as the on-chip comparator is strobed at the end of the clock period.

8.4.1.2 Fault Mode

If the voltage source applied to the $V_{IN}(+)$ or $V_{IN}(-)$ pin exceeds the allowed operating range of $V_{CC}+50$ mV, large input currents can flow through a parasitic diode to the V_{CC} pin. If these currents can exceed the 1 mA max allowed spec, an external diode (1N914) should be added to bypass this current to the V_{CC} pin (with the current bypassed with this diode, the voltage at the $V_{IN}(+)$ pin can exceed the V_{CC} voltage by the forward voltage of this diode).



Application and Implementation

NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

9.1 Application Information

The following sections give example circuits and suggestions for using the ADC080X in typical application situation with a typical 8-bit micro-processor.

9.1.1 Testing the ADC Converter

There are many degrees of complexity associated with testing an ADC converter. One of the simplest tests is to apply a known analog input voltage to the converter and use LEDs to display the resulting digital output code as shown in Figure 23.

For ease of testing, the $V_{REF}/2$ (pin 9) should be supplied with 2.560 V_{DC} and a V_{CC} supply voltage of 5.12 V_{DC} should be used. This provides an LSB value of 20 mV.

If a full-scale adjustment is to be made, an analog input voltage of 5.090 V_{DC} (5.120-1/2 LSB) should be applied to the $V_{IN}(+)$ pin with the $V_{IN}(-)$ pin grounded. The value of the $V_{REF}/2$ input voltage should then be adjusted until the digital output code is just changing from 1111 1110 to 1111 1111. This value of $V_{RFF}/2$ should then be used for all the tests.

The digital output LED display can be decoded by dividing the 8 bits into 2 hex characters, the 4 most significant (MS) and the 4 least significant (LS). Table 1 shows the fractional binary equivalent of these two 4-bit groups. By adding the voltages obtained from the "VM" and "VLS" columns in Table 1, the nominal value of the digital display (when V_{RFF}/2 = 2.560V) can be determined. For example, for an output LED display of 1011 0110 or B6 (in hex), the voltage values from the table are 3.520 + 0.120 or 3.640 V_{DC}. These voltage values represent the center-values of a perfect ADC converter. The effects of quantization error have to be accounted for in the interpretation of the test results.

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Application Information (continued)

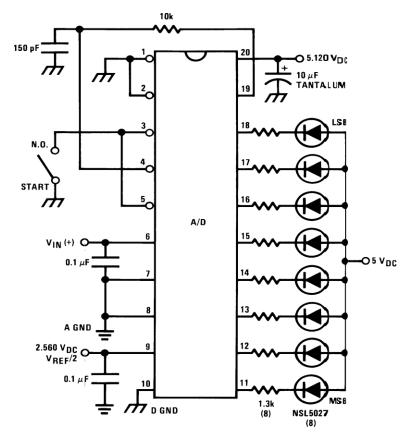


Figure 23. Basic ADC Tester

For a higher speed test system, or to obtain plotted data, a digital-to-analog converter is needed for the test setup. An accurate 10-bit DAC can serve as the precision voltage source for the ADC. Errors of the ADC under test can be expressed as either analog voltages or differences in 2 digital words.

A basic ADC tester that uses a DAC and provides the error as an analog output voltage is shown in Figure 35. The 2 op amps can be eliminated if a lab DVM with a numerical subtraction feature is available to read the difference voltage, "A–C", directly. The analog input voltage can be supplied by a low frequency ramp generator and an X-Y plotter can be used to provide analog error (Y axis) versus analog input (X axis).

For operation with a microprocessor or a computer-based test system, it is more convenient to present the errors digitally. This can be done with the circuit of Figure 25, where the output code transitions can be detected as the 10-bit DAC is incremented. This provides 1/4 LSB steps for the 8-bit ADC under test. If the results of this test are automatically plotted with the analog input on the X axis and the error (in LSB's) as the Y axis, a useful transfer function of the ADC under test results. For acceptance testing, the plot is not necessary and the testing speed can be increased by establishing internal limits on the allowed error for each code.

9.1.2 Microprocessor Interfacing

To discuss the interface with 8080A and 6800 microprocessors, a common sample subroutine structure is used. The microprocessor starts the ADC, reads and stores the results of 16 successive conversions, then returns to the user's program. The 16 data bytes are stored in 16 successive memory locations. All Data and Addresses will be given in hexadecimal form. Software and hardware details are provided separately for each type of microprocessor.



Application Information (continued)

9.1.2.1 Interfacing 8080 Microprocessor Derivatives (8048, 8085)

This converter has been designed to directly interface with derivatives of the $808\underline{0}$ microprocessor. The ADC can be mapped into memory space (using standard memory address decoding for \overline{CS} and the \overline{MEMR} and \overline{MEMW} strobes) or it can be controlled as an I/O device by using the $\overline{I/O}$ R and $\overline{I/O}$ W strobes and decoding the address bits $A0 \to A7$ (or address bits $A0 \to A15$ as they will contain the same 8-bit address information) to obtain the \overline{CS} input. Using the I/O space provides 256 additional addresses and may allow a simpler 8-bit address decoder but the data can only be input to the accumulator. To make use of the additional memory reference instructions, the ADC should be mapped into memory space. An example of an ADC in I/O space is shown in Figure 26.

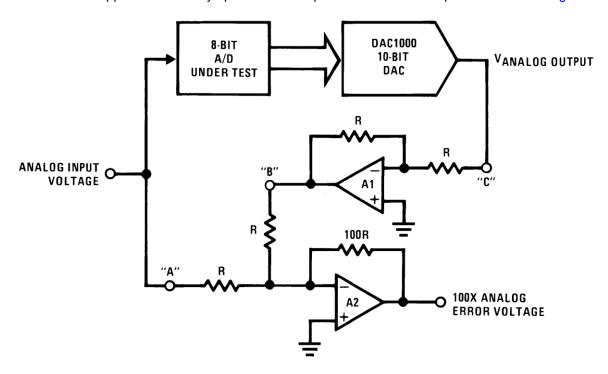


Figure 24. ADC Tester with Analog Error Output

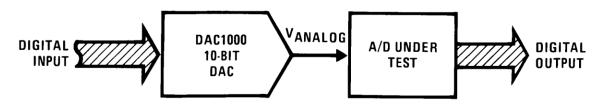


Figure 25. Basic "Digital" ADC Tester

Table 1. Decoding the Digital Output LEDs

HEX	FRACTIONAL BINARY				L BINARY VALUE F	BINARY VALUE FOR			CENTER VALUES =2.560 V _{DC}			
					MS G	MS GROUP LS G			ROUP		VMS GROUP ⁽¹⁾	VLS GROUP ⁽¹⁾
F	1	1	1	1			15/16			15/256	4.800	0.300
Е	1	1	1	0		7/8			7/128		4.480	0.280
D	1	1	0	1			13/16			13/256	4.160	0.260
С	1	1	0	0	3/4			3/64			3.840	0.240
В	1	0	1	1			11/16			11/256	3.520	0.220

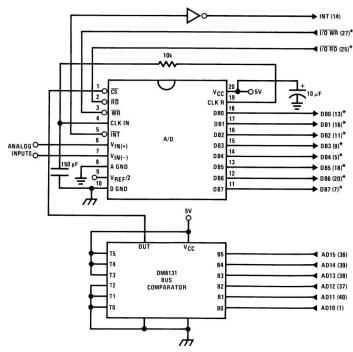
(1) Display Output=VMS Group + VLS Group



Application Information (continued)

Table 1. Decoding the Digital Output LEDs (continued)

HEX		BIN	ARY			FRACTIONAL				L BINARY VALUE FOR			OUTPUT VOLTAGE CENTER VALUES WITH V _{REF} /2=2.560 V _{DC}	
						MS G	ROUP			LS	ROUP		VMS GROUP ⁽¹⁾	VLS GROUP ⁽¹⁾
Α	1	0	1	0			5/8				5/128		3.200	0.200
9	1	0	0	1				9/16				9/256	2.880	0.180
8	1	0	0	0	1/2				1/32				2.560	0.160
7	0	1	1	1				7/16				7/256	2.240	0.140
6	0	1	1	0			3/8				3/128		1.920	0.120
5	0	1	0	1				5/16				2/256	1.600	0.100
4	0	1	0	0		1/4				1/64			1.280	0.080
3	0	0	1	1				163				3/256	0.960	0.060
2	0	0	1	0			1/8				1/128		0.640	0.040
1	0	0	0	1				1/16				1/256	0.320	0.020
0	0	0	0	0									0	0



- (1) *Pin numbers for the DP8228 system controller, others are INS8080A
- (2) Pin 23 of the INS8228 must be tied to +12V through a 1 k Ω resistor to generate the RST 7 instruction when an interrupt is acknowledged as required by the accompanying sample program.

Figure 26. ADC0801_INS8080A CPU Interface



	0038	C3 00 03	RST 7:	JMP	LD DATA	
	•	•	•			
	•	•				
Ol03	0100	21 00 02	START:	TXI H 03	H005	; HL pair will point to
NOV A, L Test # of bytes entered						; data storage locations
Olo7	0103	31 00 04	RETURN:	LXI SP (0400H	; Initialize stack pointer (Note 1)
O100	0106	7 D		MOVA, I	<u>.</u>	; Test # of bytes entered
OlOC D3 EO OUT EO H ; Start A/D OlOE FB EI ; Enable interrupt OlOF OO LOOP: NOP ; Loop until end of OllO C3 OF Ol JMP LOOP ; conversion Oll3 • CONT: • • (User program to • • • process data) • • process data) • • MOV M, A ; Store data O303 23 INX H ; Increment storage pointer	0107	FE OF		CPI OF	Ŧ	; If $\# = 16$. JMP to
O10E FB EI ; Enable interrupt O10F O0 LOOP: NOP ; Loop until end of O110 C3 OF O1 JMP LOOP ; conversion O113 • CONT: • • (User program to • • • process data) • • • • • • 0300 DB EO LD DATA: IN EO H ; Load data into accumulator O302 77 MOV M, A ; Store data O303 23 INX H ; Increment storage pointer	0109	CA 13 01		JZ CONT		; user program
010F 00 L00P: NOP ; Loop until end of	0100	D3 E0		OUT EO H	ł	; Start A/D
0110	010E	FB		EI		; Enable interrupt
Oll3	OloF	00	L00P:	NOP		; Loop until end of
(User program to process data) DBEO LD DATA: IN EO H ; Load data into accumulator MOV M, A ; Store data INX H ; Increment storage pointer	0110	C3 OF 01		JMP LOO	P	; conversion
process data) DB EO LD DATA: IN EO H ; Load data into accumulator MOV M, A ; Store data INX H ; Increment storage pointer	0113	•	CONT:	•		
process data) DB EO LD DATA: IN EO H ; Load data into accumulator MOV M, A ; Store data INX H ; Increment storage pointer	•	•	•	•		
O300 DB EO LD DATA: IN EO H ; Load data into accumulator 0302 77 MOV M, A ; Store data 0303 23 INX H ; Increment storage pointer	•	•	(User program to	•		
0302 77 MOV M, A ; Store data 0303 23 INX H ; Increment storage pointer	•	•	process data)	•		
0302 77 MOV M, A ; Store data 0303 23 INX H ; Increment storage pointer	•	•		•		
0302 77 MOV M, A ; Store data 0303 23 INX H ; Increment storage pointer	•	•	•	•		
0303 23 INXH ; Increment storage pointer	0300	DB EO	LD DATA:	IN EO H		; Load data into accumulator
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0302	77		MOV M, A	A	; Store data
0304 C3 03 01 JMP RETURN	0303	23		INXH		; Increment storage pointer
	0304	C3 03 01		JMP RET	URN	

Note: The stack pointer must be dimensioned because a RST 7 instruction pushes the PC onto the stack.

Note: All address used were arbitrarily chosen.

Figure 27. Sample Program for Figure 26 ADC0801-INS8080A CPU Interface

The standard control bus signals of the 8080 $\overline{\text{CS}}$, $\overline{\text{RD}}$ and $\overline{\text{WR}}$) can be directly wired to the digital control inputs of the ADC and the bus timing requirements are met to allow both starting the converter and outputting the data onto the data bus. A bus driver should be used for larger microprocessor systems where the data bus leaves the PCB and/or must drive capacitive loads larger than 100 pF.

9.1.2.2 Sample 8080A CPU Interfacing Circuitry and Program

The following sample program and associated hardware shown in Figure 26 may be used to input data from the converter to the INS8080A CPU chip set (comprised of the INS8080A microprocessor, the INS8228 system controller and the INS8224 clock generator). For simplicity, the ADC is controlled as an I/O device, specifically an 8-bit bi-directional port located at an arbitrarily chosen port address, E0. The Tri-state output capability of the ADC eliminates the need for a peripheral interface device, however address decoding is still required to generate the appropriate CS for the converter.

It is important to note in systems where the ADC converter is 1-of-8 or less I/O mapped devices, no address decoding circuitry is necessary. Each of the 8 address bits (A0 to A7) can be directly used as CS inputs — one for each I/O device.

9.1.2.3 INS8048 Interface

The INS8048 interface technique with the ADC0801 series (see Figure 28) is simpler than the 8080A CPU interface. There are 24 I/O lines and three test input lines in the 8048. With these extra I/O lines available, one of the I/O lines (bit 0 of port 1) is used as the chip select signal to the ADC, thus eliminating the use of an external address decoder. Bus control signals RD, WR and INT of the 8048 are tied directly to the ADC. The 16 converted data words are stored at on-chip RAM locations from 20 to 2F (Hex). The RD and WR signals are generated by reading from and writing into a dummy address, respectively. A sample interface program is shown below.



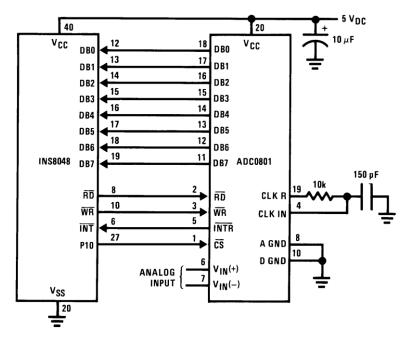


Figure 28. INS8048 Interface

04 10		JMP	10H	: Program starts at addr 10
0110		ORG	3H	
04 50		JMP	50H	: Interrupt jump vector
		ORG	10H	; Main program
99 FE		ANL	Pl, #OFEH	; Chip select
81		MOVX	A, @R1	; Read in the 1st data
				; to reset the intr
89 01	START:	ORL	P1, #1	; Set port pin high
B8 20		MOV	RO, #20H	; Data address
B9 FF		MOV	R1, #OFFH	; Dummy address
BA 10		MOA	R2, #10H	; Counter for 16 bytes
23 FF	AGAIN:	MOV	A, #OFFH	; Set ACC for intr loop
99 FE		ANL	Pl, #OFEH	; Send CS (bit 0 of Pl)
91		XVOM	@R1, A	; Send WR out
05		EN	I	; Enable interrupt
96 21	LOOP:	JNZ	LOOP	; Wait for interrupt
EA 1B		DJNZ	R2, AGAIN	; If 16 bytes are read
00		NOP		; go to user's program
00		NOP		
		ORG	50H	
81	INDATA:	MOVX	A, @Rl	; Input data, CS still low
AO		MOV	@RO, A	; Store in memory
18		INC	RO	; Increment storage counter
89 01		ORL	P1, #1	; Reset CS signal
27		CLR	A	; Clear ACC to get out of
93		RETR		; the interrupt loop

Figure 29. Sample Program for Figure 28 INS8048 Interface

9.1.2.4 Interfacing the Z-80

The Z-80 control bus is slightly different from that of the 8080. General \overline{RD} and \overline{WR} strobes are provided and separate memory request, \overline{MREQ} , and $\overline{I/O}$ request, \overline{IORQ} , signals are used which have to be combined with the generalized strobes to provide the equivalent 8080 signals. An advantage of operating the ADC in $\overline{I/O}$ space with the Z-80 is that the CPU will automatically insert one wait state (the \overline{RD} and \overline{WR} strobes are extended one clock period) to allow more time for the $\overline{I/O}$ devices to respond. Logic to map the ADC in $\overline{I/O}$ space is shown in Figure 30.



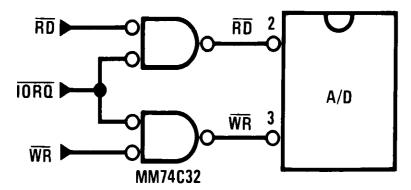


Figure 30. Mapping the ADC as an I/O Device for Use With the Z-80 CPU

Additional I/O advantages exist as software DMA routines are available and use can be made of the output data transfer which exists on the upper 8 address lines (A8 to A15) during I/O input instructions. For example, MUX channel selection for the ADC can be accomplished with this operating mode.

9.1.2.5 Interfacing 6800 Microprocessor Derivatives (6502, etc.)

The control bus for the 6800 microprocessor derivatives does not use the \overline{RD} and \overline{WR} strobe signals. Instead it employs a single R/W line and additional timing, if needed, can be derived from the $\phi 2$ clock. All I/O devices are memory mapped in the 6800 system, and a special signal, VMA, indicates that the current address is valid. Figure 36 shows an interface schematic where the ADC is memory mapped in the 6800 system. For simplicity, the \overline{CS} decoding is shown using 1/2 DM8092. Note in many 6800 systems, an already decoded $\overline{4/5}$ line is brought out to the common bus at pin 21. This can be tied directly to the \overline{CS} pin of the ADC, provided that no other devices are addressed at HX ADDR: 4XXX or 5XXX.

The following subroutine performs essentially the same function as in the case of the 8080A interface and it can be called from anywhere in the user's program.

In Figure 38 the ADC0801 series is interfaced to the M6800 microprocessor through (the arbitrarily chosen) Port B of the MC6820 or MC6821 Peripheral Interface Adapter, (PIA).

Here the $\overline{\text{CS}}$ pin of the ADC is grounded because the PIA is already memory mapped in the M6800 system and no $\overline{\text{CS}}$ decoding is necessary. Also notice that the ADC output data lines are connected to the microprocessor bus under program control through the PIA and therefore the ADC $\overline{\text{RD}}$ pin can be grounded.

A sample interface program equivalent to the previous one is shown below Figure 38. The PIA Data and Control Registers of Port B are located at HEX addresses 8006 and 8007, respectively.



9.2 Typical Applications

9.2.1 8080 Interface

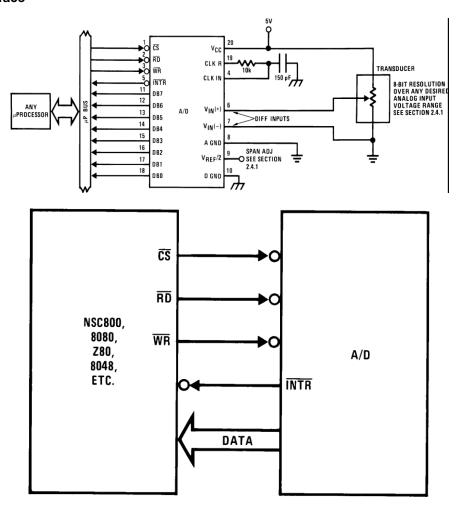


Figure 31. Generic Interface Between ADC and 8-Bit µPs

ERROR S	ERROR SPECIFICATION (Includes Full-Scale, Zero Error, and Non-Linearity)									
PART NUMBER	FULL-SCALE ADJUSTED	V _{REF} /2 = 2.500 V _{DC} (No Adjustments)	V _{REF} /2 = No Connection (No Adjustments)							
ADC0801	±1/4 LSB									
ADC0802		±1/2 LSB								
ADC0803	±1/2 LSB									
ADC0804		±1 LSB								
ADC0805			±1 LSB							

9.2.1.1 Design Requirements

For these example applications, the input analog signal is differential to illustrate the offset and common mode reduction merits. An example of the use of an adjusted reference voltage is to accommodate a reduced span or dynamic voltage range of the analog input voltage is also depicted.

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Table 2. Design Parameters

PARAMETER	EXAMPLE VALUE
ADC clock frequency, F _{CLK}	640 KHz
Input source resistance, R _{IN}	100 Ω

9.2.1.2 Detailed Design Procedure

9.2.1.2.1 Analog Differential Voltage Inputs and Common-Mode Rejection

This ADC has additional applications flexibility due to the analog differential voltage input. The $V_{IN}(-)$ input (pin 7) can be used to automatically subtract a fixed voltage value from the input reading (tare correction). This is also useful in 4 mA–20 mA current loop conversion. In addition, common-mode noise can be reduced by use of the differential input.

The time interval between sampling $V_{IN}(+)$ and $V_{IN}(-)$ is 4-1/2 clock periods. The maximum error voltage due to this slight time difference between the input voltage samples is given by:

$$\Delta V_{e} \left(MAX \right) = \left(V_{P} \right) \left(2\pi f_{cm} \right) \left(\frac{4.5}{f_{CLK}} \right)$$

where

- ΔV_e is the error voltage due to sampling delay
- V_P is the peak value of the common-mode voltage

As an example, to keep this error to 1/4 LSB (\sim 5 mV) when operating with a 60 Hz common-mode frequency, f_{cm}, and using a 640 kHz ADC clock, f_{CLK}, would allow a peak value of the common-mode voltage, V_P, which is given by:

$$V_{P} = \frac{\left[\Delta V_{e(MAX)}(f_{CLK})\right]}{(2\pi f_{cm})(4.5)}$$
(2)

or

$$V_{P} = \frac{\left(5 \times 10^{-3}\right)\left(640 \times 10^{3}\right)}{\left(6.28\right)\left(60\right)\left(4.5\right)} \tag{3}$$

which gives V_P-1.9 V.

The allowed range of analog input voltages usually places more severe restrictions on input common-mode noise levels.

An analog input voltage with a reduced span and a relatively large zero offset can be handled easily by making use of the differential input (see *Reference Voltage*).

9.2.1.2.2 Analog Inputs — Input Current

9.2.1.2.2.1 Input Bypass Capacitors

Bypass capacitors at the inputs will average these charges and cause a DC current to flow through the output resistances of the analog signal sources. This charge pumping action is worse for continuous conversions with the $V_{IN}(+)$ input voltage at full-scale. For continuous conversions with a 640 kHz clock frequency with the $V_{IN}(+)$ input at 5V, this DC current is at a maximum of approximately 5 μ A. Therefore, bypass capacitors should not be used at the analog inputs or the $V_{REF}/2$ pin for high resistance sources (> 1 k Ω). If input bypass capacitors are necessary for noise filtering and high source resistance is desirable to minimize capacitor size, the detrimental effects of the voltage drop across this input resistance, which is due to the average value of the input current, can be eliminated with a full-scale adjustment while the given source resistor and input bypass capacitor are both in place. This is possible because the average value of the input current is a precise linear function of the differential input voltage.



9.2.1.2.2.2 Input Source Resistance

Large values of source resistance where an input bypass capacitor is not used, will not cause errors as the input currents settle out prior to the comparison time. If a low pass filter is required in the system, use a low valued series resistor ($\leq 1~\text{k}\Omega$) for a passive RC section or add an op amp RC active low pass filter. For low source resistance applications, ($\leq 1~\text{k}\Omega$), a 0.1 µF bypass capacitor at the inputs will prevent noise pickup due to series lead inductance of a long wire. A 100Ω series resistor can be used to isolate this capacitor — both the R and C are placed outside the feedback loop — from the output of an op amp, if used.

9.2.1.2.2.3 Noise

The leads to the analog inputs (pins 6 and 7) should be kept as short as possible to minimize input noise coupling. Both noise and undesired digital clock coupling to these inputs can cause system errors. The source resistance for these inputs should, in general, be kept below $5 \text{ k}\Omega$. Larger values of source resistance can cause undesired system noise pickup. Input bypass capacitors, placed from the analog inputs to ground, will eliminate system noise pickup but can create analog scale errors as these capacitors will average the transient input switching currents of the ADC (see *Analog Inputs — Input Current*). This scale error depends on both a large source resistance and the use of an input bypass capacitor. This error can be eliminated by doing a full-scale adjustment of the ADC (adjust $V_{REF}/2$ for a proper full-scale reading — see *Full-Scale*) with the source resistance and input bypass capacitor in place.

Noise spikes on the V_{CC} supply line can cause conversion errors as the comparator will respond to this noise. A low inductance tantalum filter capacitor should be used close to the converter V_{CC} pin and values of 1 μ F or greater are recommended. If an unregulated voltage is available in the system, a separate LM340LAZ-5.0, TO-92, 5-V voltage regulator for the converter (and other analog circuitry) will greatly reduce digital noise on the V_{CC} supply.

9.2.1.2.3 Reference Voltage

9.2.1.2.3.1 Span Adjust

For maximum applications flexibility, these ADCs have been designed to accommodate a 5 V_{DC} , 2.5 V_{DC} or an adjusted voltage reference. This has been achieved in the design of the IC as shown in Figure 32.

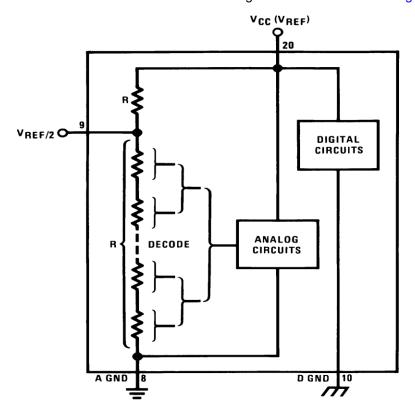


Figure 32. The V_{REFERENCE} Design on the IC

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Notice that the reference voltage for the IC is either 1/2 of the voltage applied to the V_{CC} supply pin, or is equal to the voltage that is externally forced at the $V_{REF}/2$ pin. This allows for a ratiometric voltage reference using the V_{CC} supply, a 5 V_{DC} reference voltage can be used for the V_{CC} supply or a voltage less than 2.5 V_{DC} can be applied to the $V_{REF}/2$ input for increased application flexibility. The internal gain to the $V_{REF}/2$ input is 2, making the full-scale differential input voltage twice the voltage at pin 9.

An example of the use of an adjusted reference voltage is to accommodate a reduced span — or dynamic voltage range of the analog input voltage. If the analog input voltage were to range from 0.5 V_{DC} to 3.5 V_{DC} , instead of 0V to 5 V_{DC} , the span would be 3 V as shown in Figure 33. With 0.5 V_{DC} applied to the $V_{IN}(-)$ pin to absorb the offset, the reference voltage can be made equal to 1/2 of the 3V span or 1.5 VDC. The ADC now will encode the $V_{IN}(+)$ signal from 0.5V to 3.5 V with the 0.5V input corresponding to zero and the 3.5 VDC input corresponding to full-scale. The full 8 bits of resolution are therefore applied over this reduced analog input voltage range.

9.2.1.2.3.2 Reference Accuracy Requirements

The converter can be operated in a ratiometric mode or an absolute mode. In ratiometric converter applications, the magnitude of the reference voltage is a factor in both the output of the source transducer and the output of the ADC converter and therefore cancels out in the final digital output code. The ADC0805 is specified particularly for use in ratiometric applications with no adjustments required. In absolute conversion applications, both the initial value and the temperature stability of the reference voltage are important factors in the accuracy of the ADC converter. For $V_{REF}/2$ voltages of 2.4 V_{DC} nominal value, initial errors of ±10 m V_{DC} will cause conversion errors of ±1 LSB due to the gain of 2 of the $V_{REF}/2$ input. In reduced span applications, the initial value and the stability of the $V_{REF}/2$ input voltage become even more important. For example, if the span is reduced to 2.5 V, the analog input LSB voltage value is correspondingly reduced from 20 mV (5V span) to 10 mV and 1 LSB at the $V_{REF}/2$ input becomes 5 mV. As can be seen, this reduces the allowed initial tolerance of the reference voltage and requires correspondingly less absolute change with temperature variations. Note that spans smaller than 2.5 V place even tighter requirements on the initial accuracy and stability of the reference source.

In general, the magnitude of the reference voltage will require an initial adjustment. Errors due to an improper value of reference voltage appear as full-scale errors in the ADC transfer function. IC voltage regulators may be used for references if the ambient temperature changes are not excessive. The LM336B 2.5-V IC reference diode (from National Semiconductor) has a temperature stability of 1.8 mV typical (6 mV maximum) over $0^{\circ}C \le T_A \le +70^{\circ}C$. Other temperature range parts are also available.

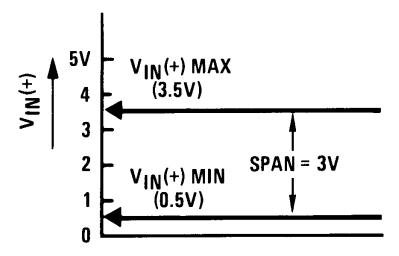
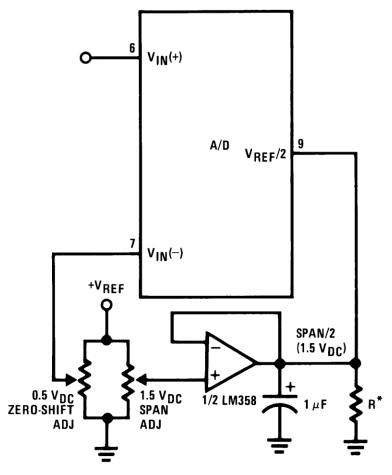


Figure 33. Analog Input Signal Example





*Add if VREF/2 ≤ 1 VDC with LM358 to draw 3 mA to ground.

Figure 34. Accommodating an Analog Input from 0.5V (Digital Out = 00_{HEX}) to 3.5 V (Digital Out= FF_{HEX})

9.2.1.2.4 Errors and Reference Voltage Adjustments

9.2.1.2.4.1 Zero Error

The zero of the ADC does not require adjustment. If the minimum analog input voltage value, $V_{IN(MIN)}$, is not ground, a zero offset can be done. The converter can be made to output 0000 0000 digital code for this minimum input voltage by biasing the ADC $V_{IN}(-)$ input at this $V_{IN}(MIN)$ value (see *Application Information*). This uses the differential mode operation of the ADC.

The zero error of the ADC converter relates to the location of the first riser of the transfer function and can be measured by grounding the $V_{IN}(-)$ input and applying a small magnitude positive voltage to the $V_{IN}(+)$ input. Zero error is the difference between the actual DC input voltage that is necessary to just cause an output digital code transition from 0000 0000 to 0000 0001 and the ideal 1/2 LSB value (1/2 LSB = 9.8 mV for $V_{REF}/2=2.500 V_{DC}$).

9.2.1.2.4.2 Full-Scale

The full-scale adjustment can be made by applying a differential input voltage that is 11/2 LSB less than the desired analog full-scale voltage range and then adjusting the magnitude of the $V_{REF}/2$ input (pin 9 or the V_{CC} supply if pin 9 is not used) for a digital output code that is just changing from 1111 1110 to 1111 1111.



9.2.1.2.4.3 Adjusting for an Arbitrary Analog Input Voltage Range

If the analog zero voltage of the ADC is shifted away from ground (for example, to accommodate an analog input signal that does not go to ground) this new zero reference should be properly adjusted first. A $V_{IN}(+)$ voltage that equals this desired zero reference plus 1/2 LSB (where the LSB is calculated for the desired analog span, 1 LSB=analog span/256) is applied to pin 6 and the zero reference voltage at pin 7 should then be adjusted to just obtain the 00_{HEX} to 01_{HEX} code transition.

The full-scale adjustment should then be made (with the proper $V_{IN}(-)$ voltage applied) by forcing a voltage to the $V_{IN}(+)$ input which is given by:

$$V_{IN}\left(+\right) \text{fs adj} = V_{MAX} - 1.5 \left[\frac{\left(V_{MAX} - V_{MIN}\right)}{256} \right]$$

where

- V_{MAX} = The high end of the analog input range
- V_{MIN} = the low end (the offset zero) of the analog range. (Both are ground referenced.)

The $V_{REF}/2$ (or V_{CC}) voltage is then adjusted to provide a code change from FE_{HEX} to FF_{HEX} . This completes the adjustment procedure

9.2.1.2.5 Clocking Option

The clock for the ADC can be derived from the CPU clock or an external RC can be added to provide self-clocking. The CLK IN (pin 4) makes use of a Schmitt trigger as shown in Figure 35.

$$f_{CLK} = \frac{1}{RC \ In \left[\left(\frac{V_{CC} - V_{T^{-}}}{V_{CC} - V_{T^{+}}} \right) \left(\frac{V_{T^{+}}}{V_{T^{-}}} \right) \right]}$$

 $R \simeq 10 \text{ k}\Omega$

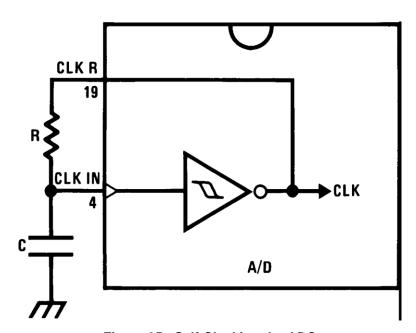


Figure 35. Self-Clocking the ADC

Heavy capacitive or DC loading of the clock R pin should be avoided as this will disturb normal converter operation. Loads less than 50 pF, such as driving up to 7 ADC converter clock inputs from a single clock R pin of 1 converter, are allowed. For larger clock line loading, a CMOS or low power TTL buffer or PNP input logic should be used to minimize the loading on the clock R pin (do not use a standard TTL buffer).



9.2.1.2.6 Restart During a Conversion

If the ADC is restarted $\overline{(CS)}$ and \overline{WR} go low and return high) during a conversion, the converter is reset and a new conversion is started. The output data latch is not updated if the conversion in process is not allowed to be completed, therefore the data of the previous conversion remains in this latch. The \overline{INTR} output simply remains at the "1" level.

9.2.1.2.7 Continuous Conversions

For operation in the free-running mode an initializing pulse should be used, following <u>power</u> up, to ensure <u>circuit operation</u>. In this application, the <u>CS</u> input is grounded and the <u>WR</u> input is tied to the <u>INTR</u> output. This <u>WR</u> and <u>INTR</u> node should be momentarily forced to logic low following a power-up cycle to ensure operation.

9.2.1.2.8 Driving the Data Bus

This MOS ADC, like MOS microprocessors and memories, will require a bus driver when the total capacitance of the data bus gets large. Other circuitry, which is tied to the data bus, will add to the total capacitive loading, even in Tri-state (high impedance mode). Backplane bussing also greatly adds to the stray capacitance of the data bus.

There are some alternatives available to the designer to handle this problem. Basically, the capacitive loading of the data bus slows down the response time, even though DC specifications are still met. For systems operating with a relatively slow CPU clock frequency, more time is available in which to establish proper logic levels on the bus and therefore higher capacitive loads can be driven (see typical characteristics curves).

At higher CPU clock frequencies time can be extended for I/O reads (and/or writes) by inserting wait states (8080) or using clock extending circuits (6800).

Finally, if time is short and capacitive loading is high, external bus drivers must be used. These can be Tri-state buffers (low power Schottky such as the DM74LS240 series is recommended) or special higher drive current products which are designed as bus drivers. High current bipolar bus drivers with PNP inputs are recommended.

9.2.1.2.9 Wiring and Hook-Up Precautions

Standard digital wire wrap sockets are not satisfactory for breadboarding this ADC converter. Sockets on PCBs can be used and all logic signal wires and leads should be grouped and kept as far away as possible from the analog signal leads. Exposed leads to the analog inputs can cause undesired digital noise and hum pickup, therefore shielded leads may be necessary in many applications.

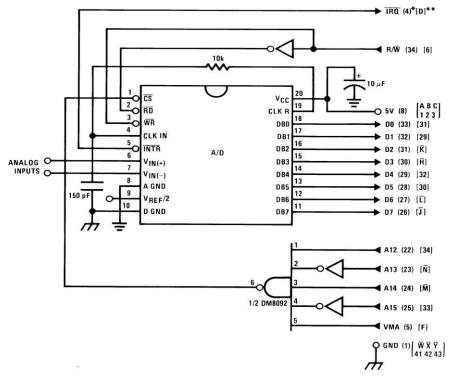
A single point analog ground that is separate from the logic ground points should be used. The power supply bypass capacitor and the self-clocking capacitor (if used) should both be returned to digital ground. Any $V_{REF}/2$ bypass capacitors, analog input filter capacitors, or input signal shielding should be returned to the analog ground point. A test for proper grounding is to measure the zero error of the ADC converter. Zero errors in excess of 1/4 LSB can usually be traced to improper board layout and wiring (see *Zero Error* for measuring the zero error).

9.2.2 Multiple ADC0801 Series to MC6800 CPU Interface

To transfer analog data from several channels to a single microprocessor system, a multiple converter scheme presents several advantages over the conventional multiplexer single-converter approach. With the ADC0801 series, the differential inputs allow individual span adjustment for each channel. Furthermore, all analog input channels are sensed simultaneously, which essentially divides the total system servicing time of the microprocessor by the number of channels, because all conversions occur simultaneously. This scheme is shown in Figure 40.

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^{*}Numbers in parentheses refer to MC6800 CPU pin out.

Figure 36. ADC0801-MC6800 CPU Interface

ents of X ow CPU 02C
02C
0801
nterrupt
ata stored?
ADC0801
t X
address for
age
ize TEMP1
om subroutine
program
a

In order for the microprocessor to service subroutines and inter- rupts, the stack pointer must be dimensioned in the user's program.

Figure 37. Sample Program for Figure 36 ADC0801-MC6800 CPU Interface

^{**}Number or letters in brackets refer to standard M6800 system common bus code.



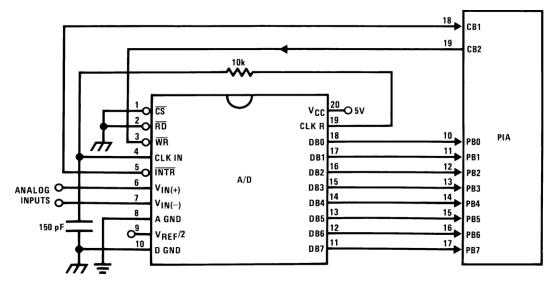


Figure 38. ADC0801-MC6820 PIA Interface

0010	CE 00 38	DATAIN	LDX	#\$0038	; Upon IRQ low CPU
0013	FF FF F8		STX	\$FFF8	; jumps to 0038
0016	B6 80 06		LDAA	PIAORB	; Clear possible IRQ flags
0019	4F		CLRA		
001A	B7 80 07		STAA	PIACRB	
001D	B7 80 06		STAA	PIAORB	; Set Port Bas input
0020	OE		CLI		
0021	C6 34		LDAB	#\$34	
0023	86 3D		LDAA	#\$3D	
0025	F7 80 07	CONVRT	STAB	PIACRB	; Starts ADC0801
0028	B7 80 07		STAA	PIACRB	
002B	3E		WAI		; Wait for interrupt
0020	DE 40		LDX	TEMPl	
002E	8C 02 0F		CPX	#\$020F	; Is final data stored?
0031	27 OF		BEQ	ENDP	
0033	08		INX		
0034	DF 40		STX	TEMPl	
0036	20 ED		BRA	CONVRT	
0038	DE 40	INTRPT	LDX	TEMPl	
003A	B6 80 06		LDAA	PIAORB	; Read data in
003D	A7 00		STAA	x	; Store it at X
003F	3B		RTI		
0040	02 00	TEMP1	FDB	\$0200	; Starting address for
					; data storage
0042	CE 02 00	ENDP	LDX	#\$0200	; Reinitialize TEMP1
0045	DF 40		STX	TEMP1	
0047	39		RTS		; Return from subroutine
		PIAORB	EQU	\$8006	; To user's program
		PIACRB	EQU	\$8007	

Figure 39. Sample Program for Figure 38 ADC0801–MC6820 PIA Interface

The following schematic and sample subroutine (DATA IN) in *Auto-Zeroed Differential Transducer Amplifier and ADC Converter* section may be used to interface (up to) 8 ADC0801's directly to the MC6800 CPU. This scheme can easily be extended to allow the interface of more converters. In this configuration the converters are (arbitrarily) located at HEX address 5000 in the MC6800 memory space. To save components, the clock signal is derived from just one RC pair on the first converter. This output drives the other ADCs.

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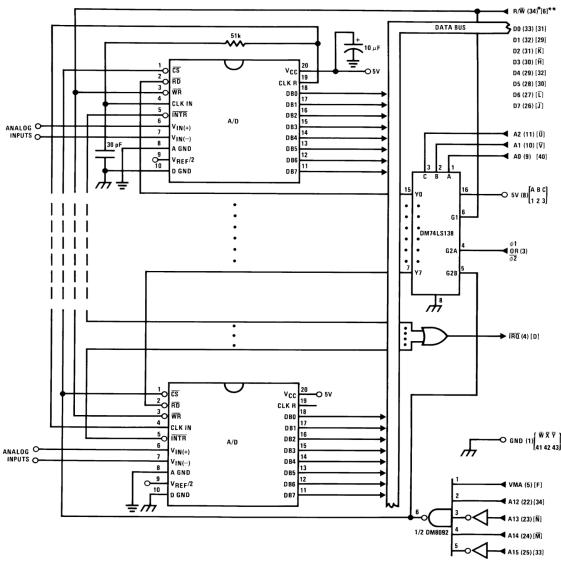


All the converters are started simultaneously with a STORE instruction at HEX address 5000. Note any other HEX address of the form 5XXX will be decoded by the circuit, pulling all the CS inputs low. This can easily be avoided by using a more definitive address decoding scheme. All the interrupts are ORed together to insure that all ADCs have completed their conversion before the microprocessor is interrupted.

The subroutine, DATA IN, may be called from anywhere in the user's program. Once called, this routine initializes the CPU, starts all the converters simultaneously and waits for the interrupt signal. Upon receiving the interrupt, it reads the converters (from HEX addresses 5000 through 5007) and stores the data successively at (arbitrarily chosen) HEX addresses 0200 to 0207, before returning to the user's pro- gram. All CPU registers then recover the original data they had before servicing DATA IN.

9.2.3 Auto-Zeroed Differential Transducer Amplifier and ADC Converter

The differential inputs of the ADC0801 series eliminate the need to perform a differential to single ended conversion for a differential transducer. Thus, one op amp can be eliminated because the differential to single ended conversion is provided by the differential input of the ADC0801 series. In general, a transducer preamp is required to take advantage of the full ADC converter input dynamic range.



^{*}Numbers in parentheses refer to MC6800 CPU pin out.

Figure 40. Interfacing Multiple ADCs in an MC6800 System

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^{**}Numbers of letters in brackets refer to standard M6800 system common bus code.



ADDRESS	HEX CODE		MNEMONICS		COMMENTS
0010	DF 44	DATAIN	STX	TEMP	; Save Contents of X
0012	CE 00 2A		LDX	#\$002A	; Upon IRQ LOW CPU
0015	FF FF F8		STX	\$FFF8	; Jumps to 002A
0018	B7 50 00		STAA	\$5000	;Starts all A/D's
001B	OE		CLI		
001C	3E		WAI		; Wait for interrupt
001D	CE 50 00		LDX	#\$5000	
0020	DF 40		STX	INDEX1	; Reset both INDEX
0022	CE 02 00		LDX	#\$0200	; 1 and 2 to starting
0025	DF 42		STX	INDEX2	; addresses
0027	DE 44		LDX	TEMP	
0029	39		RTS		; Return from subroutine
002A	DE 40	INTRPT	LDX	INDEX1	; INDEX1 \rightarrow X
002C	A6 00		LDAA	Х	; Read data in from A/D at X
002E	08		INX		; Increment X by one
002F	DF 40		STX	INDEX1	$; X \rightarrow INDEX1$
0031	DE 42		LDX	INDEX2	; INDEX2 \rightarrow X

Figure 41. Sample Program for Figure 40 Interfacing Multiple ADC's in an MC6800 System

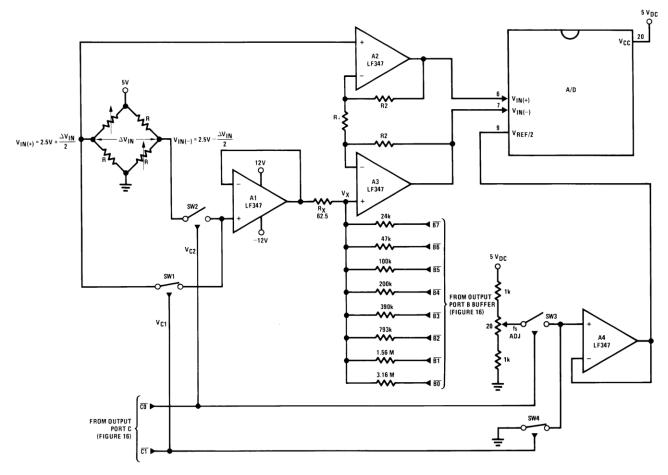
ADDRESS	HEX CODE	I	MNEMONIC	S	COMMENTS
0033	A7 00		STAA	X	; Store data at X
0035	8C 02 07		CPX	#\$0207	; Have all A/D's been read?
0038	27 05		BEQ	RETURN	; Yes: branch to RETURN
003A	08		INX		; No: increment X by one
003B	DF 42		STX	INDEX2	$; X \rightarrow INDEX2$
003D	20 EB		BRA	INTRPT	; Branch to 002A
003F	3B	RETURN	RTI		
0040	50 00	INDEX1	FDB	\$5000	; Starting address for A/D
0042	02 00	INDEX2	FDB	\$0200	; Starting address for data storage
0044	00 00	TEMP	FDB	\$0000	

Figure 42. Sample Program for Figure 40 Interfacing Multiple ADC's in an MC6800 System

Note: In order for the microprocessor to service subroutines and interrupts, the stack pointer must be dimensioned in the user's program.

For amplification of DC input signals, a major system error is the input offset voltage of the amplifiers used for the preamp. Figure 43 is a gain of 100 differential preamp whose offset voltage errors will be cancelled by a zeroing subroutine which is performed by the INS8080A microprocessor system. The total allowable input offset voltage error for this preamp is only 50 μ V for ℓ 4 LSB error. This would obviously require very precise amplifiers. The expression for the differential output voltage of the preamp is:





R2 = 49.5 R1

Switches are LMC13334 CMOS analog switches.

The 9 resistors used in the auto-zero section can be ±5% tolerance.

Figure 43. Gain of 100 Differential Transducer Preamp

$$V_{O} = \underbrace{\left[V_{IN}\left(+\right) - V_{IN}\left(-\right)\right]}_{SIGNAL} \underbrace{\left[1 + \frac{2R2}{R1}\right]}_{GAIN} + \underbrace{\left(V_{OS_{2}} - V_{OS_{1}} - V_{OS_{3}} \pm I_{X}R_{X}\right)}_{DC \ ERROR \ TERM} \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{GAIN} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{GAIN} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{DC \ ERROR \ TERM} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{GAIN} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{DC \ ERROR \ TERM} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{GAIN} + \underbrace{\left(1 + \frac{2R2}{R1}\right)}_{DC \ ERROR \ TERM} + \underbrace{$$

where

• I_X is the current through resistor R_X

(5)

All of the offset error terms can be cancelled by making $\pm I_X R_X = V_{OS1} + V_{OS3} - V_{OS2}$. This is the principle of this auto-zeroing scheme.

The INS8080A uses the 3 I/O ports of an INS8255 Programable Peripheral Interface (PPI) to control the auto zeroing and input data from the ADC0801 as shown in Figure 44. The PPI is programmed for basic I/O operation (mode 0) with Port A being an input port and Ports B and C being output ports. Two bits of Port C are used to alternately open or close the 2 switches at the input of the preamp. Switch SW1 is closed to force the preamp's differential input to be zero during the zeroing subroutine and then opened and SW2 is then closed for conversion of the actual differential input signal. Using 2 switches in this manner eliminates concern for the ON resistance of the switches as they must conduct only the input bias current of the input amplifiers.



Output Port B is used as a successive approximation register by the 8080 and the binary scaled resistors in series with each output bit create a D/A converter. During the zeroing subroutine, the voltage at V_x increases or decreases as required to make the differential output voltage equal to zero. This is accomplished by ensuring that the voltage at the output of A1 is approximately 2.5V so that a logic "1" (5V) on any output of Port B will source current into node V_X thus raising the voltage at V_X and making the output differential more negative. Conversely, a logic "0" (0V) will pull current out of node V_X and decrease the voltage, causing the differential output to become more positive. For the resistor values shown, V_X can move ±12 mV with a resolution of 50 μ V, which will null the offset error term to ℓ 4 LSB of full-scale for the ADC0801. It is important that the voltage levels that drive the auto-zero resistors be constant. Also, for symmetry, a logic swing of 0V to 5V is convenient. To achieve this, a CMOS buffer is used for the logic output signals of Port B and this CMOS package is powered with a stable 5V source. Buffer amplifier A1 is necessary so that it can source or sink the D/A output current.

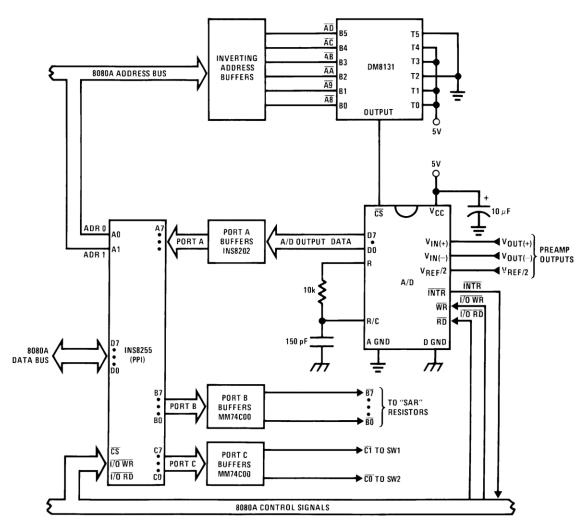


Figure 44. Microprocessor Interface Circuitry for Differential Preamp

A flow chart for the zeroing subroutine is shown in Figure 45. It must be noted that the ADC0801 series will output an all zero code when it converts a negative input $[V_{IN}(-) \ge V_{IN}(+)]$. Also, a logic inversion exists as all of the I/O ports are buffered with inverting gates.

Basically, if the data read is zero, the differential output voltage is negative, so a bit in Port B is cleared to pull VX more negative which will make the output more positive for the next conversion. If the data read is not zero, the output voltage is positive so a bit in Port B is set to make VX more positive and the output more negative. This continues for 8 approximations and the differential output eventually converges to within 5 mV of zero.

The actual program is given in Figure 46. All addresses used are compatible with the BLC 80/10 microcomputer system. In particular:



www ti com

- Port A and the ADC0801 are at port address E4
- · Port B is at port address E5
- Port C is at port address E6
- PPI control word port is at port address E7
- Program Counter automatically goes to ADDR:3C3D upon acknowledgment of an interrupt from the ADC0801

9.2.4 Multiple ADC Converters in a Z-80 Interrupt Driven Mode

In data acquisition systems where more than one ADC converter (or other peripheral device) will be interrupting program execution of a microprocessor, there is obviously a need for the CPU to determine which device requires servicing. Figure 47 and the accompanying software is a method of determining which of 7 ADC0801 converters has completed a conversion (INTR asserted) and is requesting an interrupt. This circuit allows starting the ADC converters in any sequence, but will input and store valid data from the converters with a priority sequence of ADC 1 being read first, ADC 2 second, etc., through ADC 7 which would have the lowest priority for data being read. Only the converters whose INT is asserted will be read.

The key to decoding circuitry is the DM74LS373, 8-bit D type flip-flop. When the Z-80 acknowledges the interrupt, the program is vectored to a data input Z-80 subroutine. This subroutine will read a peripheral status word from the DM74LS373 which contains the logic state of the INTR outputs of all the converters. Each converter which initiates an interrupt will place a logic "0" in a unique bit position in the status word and the subroutine will determine the identity of the converter and execute a data read. An identifier word (which indicates which ADC the data came from) is stored in the next sequential memory location above the location of the data so the program can keep track of the identity of the data entered.



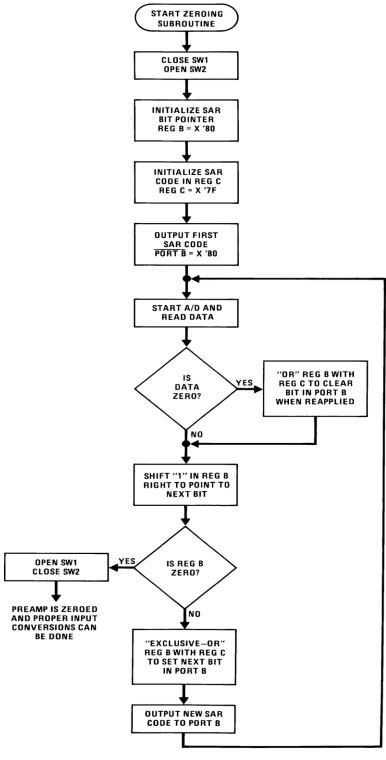


Figure 45. Flow Chart for Auto-Zero Routine



3D00	3E90	MVI 90		
3D02	D3E7	Out Control Port		; Program PPI
3D04	2601	MVI H Ol	Auto-Zero Subroutine	,
3D06	7C	MOV A, H		
3D07	D3E6	OUT C		; Close SW1 open SW2
3D09	0680	MVI B 80		; Initialize SAR bit pointer
3DOB	3E7F	MVI A 7F		: Initialize SAR code
3DOD	4F	MOV C, A	Return	,
3DOE	D3E5	OUT B		; Port B = SAR code
3D10	31AA3D	LXI SP 3DAA	Start	; Dimension stack pointer
3D13	D3E4	OUT A	2 3 3 3 3	; Start A/D
3D15	FB	IE		, 5001011/5
3D16	00	NOP	Loop	; Loop until INT asserted
3D17	C3163D	JMP Loop		, zoop until ini abboi tod
3D1A	7A	MOV A.D	Auto-Zero	
3D1B	C600	ADI OO		
3D1D	CA2D3D	JZ Set C		; Test A/D output data for zero
3D20	78	MOV A, B	Shift B	, ==== 1, = ===========================
3D21	F600	ORI OO		; Clear carry
3D23	1F	RAR		; Shift "1" in B right one place
3D24	FEOO	CPI 00		; Is B zero? If yes last
3D26	CA373D	JZ Done		; approximation has been made
3D29	47	MOV B, A		,
3D2A	C3333D	JMP New C		
3D2D	79	MOV A, C	Set C	
3D2E	во	ORA B		; Set bit in C that is in same
3D2F	4F	MOV C, A		; position as "l" in B
3D30	C3203D	JMP Shift B		ta t y is classed as streams
3D33	A9	XRA C	New C	; Clear bit in C that is in
3D34	C30D3D	JMP Return		; same position as "l" in B
3D37	47	MOV B, A	Done	; then output new SAR code.
3D38	7C	MOV A, H		; Open SW1, close SW2 then
3D39	EE03	XRI 03		; proceed with program. Preamp
3D3B	D3E6	OUT C		; is now zeroed.
3D3D		•	Normal	
		•		
		•		
		Program for processing		
		proper data values		
3C3D	DBE4	INA	Read A/D Subroutine	; Read A/D data
3C3F	EEFF	XRI FF		; Invert data
3041	57	MOV D, A		
3C42	78	MOV A, B		; Is B Reg = 0? If not stay
3043	E6FF	ANI FF		; in auto zero subroutine
3C45	C21A3D	JNZ Auto-Zero		
3048	C33D3D	JMP Normal		

NOTE: All numerical values are hexadecimal representations.

Figure 46. Software for Auto-Zeroed Differential ADC

The following notes apply:

- It is assumed that the CPU automatically performs a RST 7 instruction when a valid interrupt is acknowledged (CPU is in interrupt mode 1). Hence, the subroutine starting address of X0038.
- The address bus from the Z-80 and the data bus to the Z-80 are assumed to be inverted by bus drivers.
- ADC data and identifying words will be stored in sequential memory locations starting at the arbitrarily chosen address X 3E00.
- The stack pointer must be dimensioned in the main program as the RST 7 instruction automatically pushes
 the PC onto the stack and the subroutine uses an additional 6 stack addresses.
- The peripherals of concern are mapped into I/O space with the following port assignments:

Table 3. Port Assignment Where Peripherals are Mapped into I/O Space

HEX PORT ADDRESS	PERIPHERAL	HEX PORT ADDRESS	PERIPHERAL
00	MM74C374 8-bit flip-flop	04	ADC 4
01	ADC 1	05	ADC 5



Table 3. Port Assignment Where Peripherals are Mapped into I/O Space (continued)

HEX PORT ADDRESS	PERIPHERAL	HEX PORT ADDRESS	PERIPHERAL
02	ADC 2	06	ADC 6
03	ADC 3	07	ADC 7

This port address also serves as the ADC identifying word in the program.

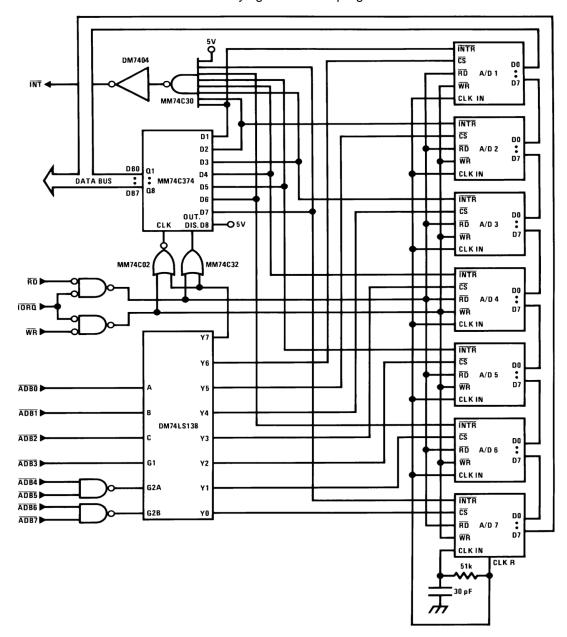


Figure 47. Multiple ADCs With Z-80 Type Microprocessor



INTERRUPT SERVICING SUBROUTINE

			SOURCE	
LOC	OBJ CODE		STATEMENT	COMMENT
0038	E5		PUSH HL	; Save contents of all registers affected by
0039	C5		PUSH BC	; this subroutine.
003A	F5		PUSH AF	; Assumed INT mode learlier set.
003B	21 00 3E		LD (HL), X3E00	; Initialize memory pointer where data will be stored.
003E	OE 01		LD C, XO1	; C register will be port ADDR of A/D converters.
0040	D300		OUT XOO, A	; Load peripheral status word into 8-bit latch.
0042	DB00		INA, XOO	; Load status word into accumulator.
0044	47		LD B, A	; Save the status word.
0045	79	TEST	LDA,C	; Test to see if the status of all A/D's have
0046	FE 08		CP, X08	; been checked. If so, exit subroutine
0048	CA 60 00		JPZ, DONE	
004B	78		LD A, B	; Test a single bit in status word by looking for
004C	1F		RRA	; a "1" to be rotated into the CARRY (an INT
004D	47		LD B, A	; is loaded as a "l"). If CARRY is set then load
004E	DA 5500		JPC, LOAD	; contents of A/D at port ADDR in C register.
0051	OC	NEXT	INC C	; If CARRY is not set, increment C register to point
0052	C3 4500		JP, TEST	; to next A/D, then test next bit in status word.
0055	ED 78	LOAD	IN A, (C)	; Read data from interrupting A/D and invert
0057	EE FF		XOR FF	; the data.
0059	77		LD (HL),A	; Store the data
005A	20		INC L	
005B	71		LD (HL),C	; Store A/D identifier (A/D port ADDR).
005C	20		INCL	
005D	C3 51 00		JP, NEXT	; Test next bit in status word.
0060	Fl	DONE	POP AF	; Re-establish all registers as they were
0061	Cl		POP BC	; before the interrupt.
0062	El		POP HL	A consideration and the contraction of the contract
0063	C9		RET	; Return to original program



9.3 System Examples

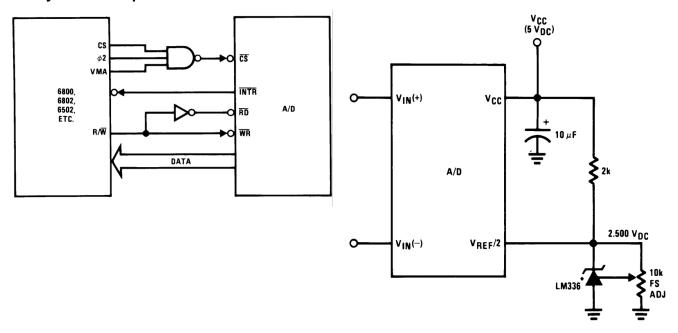


Figure 48. 6800 Interface

*For low power, see also LM385–2.5

Figure 49. Absolute With a 2.5-V Reference

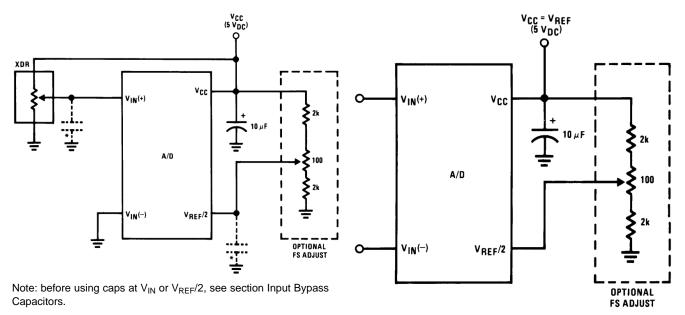


Figure 50. Ratiometeric With Full-Scale Adjust

Figure 51. Absolute With a 5-V Reference



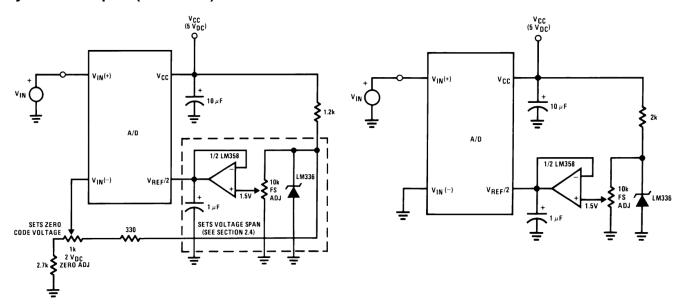


Figure 52. Zero-Shift and Span Adjust: 2 V \leq V_{IN} \leq 5

Figure 53. Span Adjust: $0 \text{ V} \leq V_{IN} \leq 3 \text{ V}$

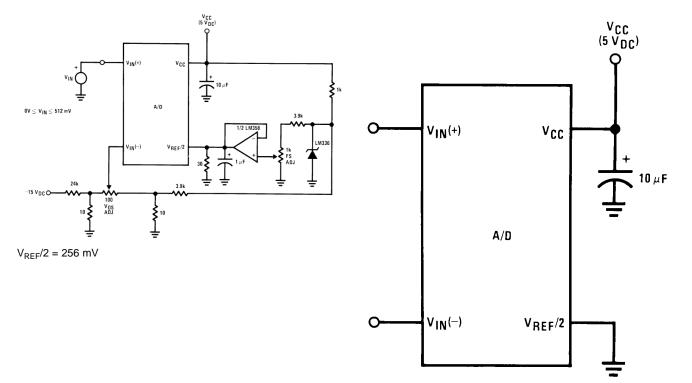
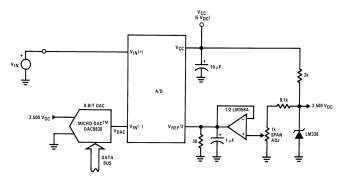


Figure 54. Directly Converting a Low-Level Signal

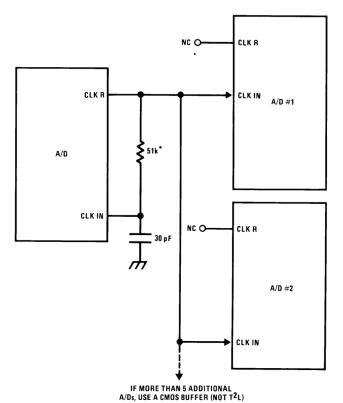
Figure 55. A µP Interfaced Comparator

For: $V_{IN}(+)>V_{IN}(-)$; Output = FF_{HEX} For: $V_{IN}(+) < V_{IN}(-)$; Output = 00_{HEX}



 $V_{REF}/2{=}128$ mV; 1 LSB =1 mV; $V_{DAC} \leq V_{IN} \leq (V_{DAC} + 256$ mV); 0 \leq $V_{DAC} < 2.5$ V

Figure 56. 1-mV Resolution With μP-Controlled Range



^{*} Use a large R value to reduce loading at CLK R output.

Figure 58. Self-Clocking Multiple ADCs

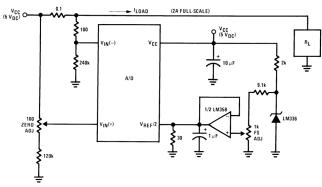
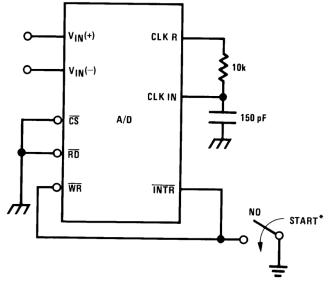


Figure 57. Digitizing a Current Flow



*After power up, a momentary grounding of the WR input is needed to ensure operation.

Figure 59. Self-Clocking in Free-Running Mode



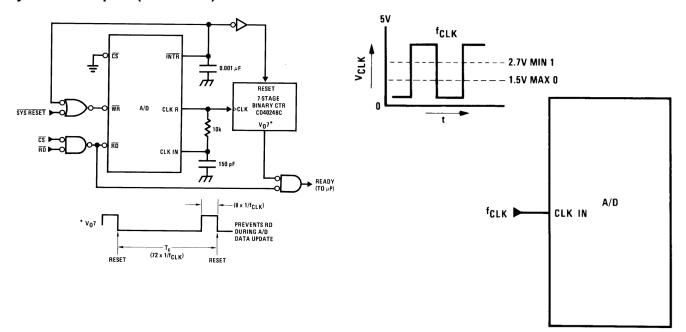
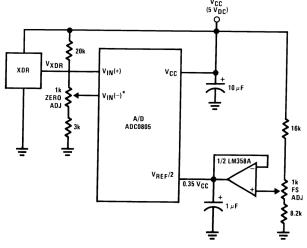


Figure 60. µP Interface for Free-Running ADC

100 kHz ≤ f_{CLK} ≤ 1460 kHz Figure 61. External clocking



 $^*_{VIN}(\neg) = 0.15 \ V_{CC}$ 15% of $V_{CC} \le V_{XDR} \le 85\%$ of V_{CC}

Figure 62. Operating With "Automotive" Ratiometric Transducers

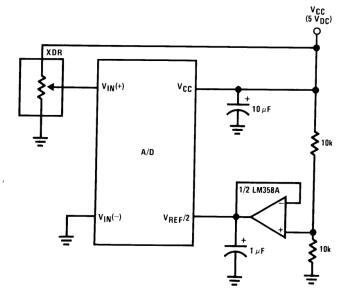
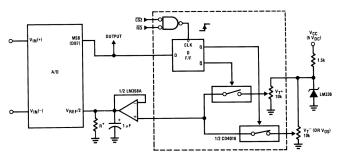


Figure 63. Ratiometric With V_{REF}/2 Forced





*Select R value DB7 = "1" for $V_{IN}(+)>V_{IN}(-)+(V_{REF}/2)$. Omit circuitry within the dotted area if hysteresis is not needed.

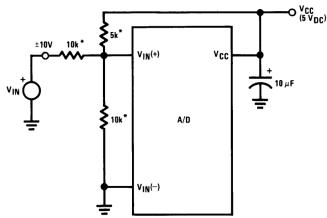


Figure 65. Handling ±10-V Analog Inputs

*Beckman Instruments #694-3-R10K resistor array

Figure 64. μP-Compatible Differential-Input Comparator With Pre-Set VOS (With or Without Hysteresis)

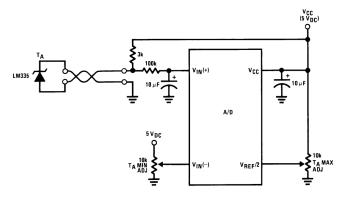
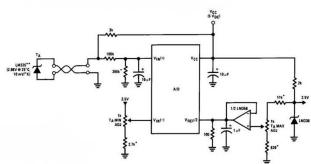


Figure 66. Low-Cost, µP-Interfaced, Temperature-to-Digital Converter



**Can calibrate each sensor to allow easy replacement, then ADC can be calibrated with a pre-set input voltage.

Figure 67. µP-Interfaced Temperature-to-Digital Converter



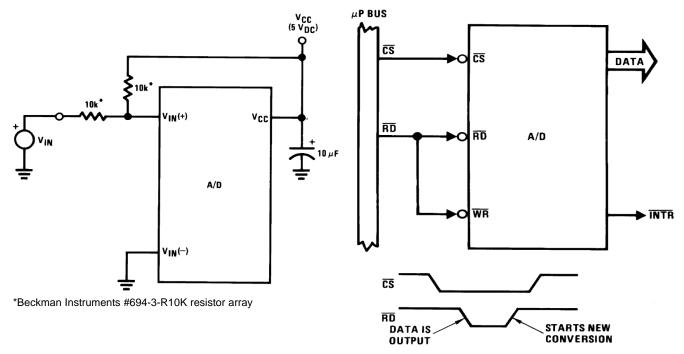


Figure 68. Handling ±5-V Analog Inputs

Figure 69. Read-Only Interface

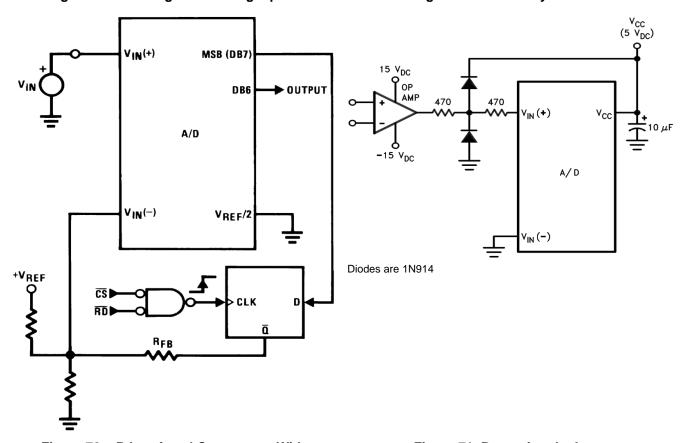
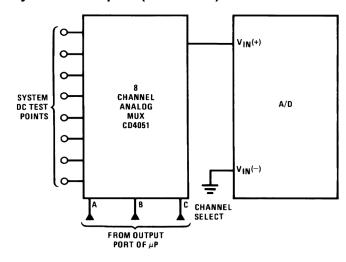


Figure 70. µP-Interfaced Comparator With Hysteresis

Figure 71. Protecting the Input

TEXAS INSTRUMENTS

System Examples (continued)



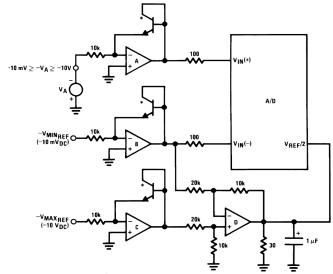
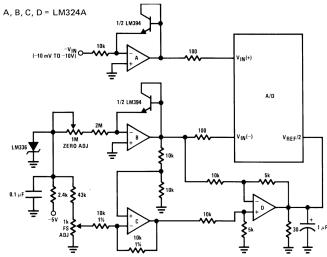


Figure 72. Analog Self-Test for a System

*LM389 transistors A, B, C, D = LM324A quad op amp

Figure 73. A Low-Cost, 3-Decade Logarithmic Converter



f_C=20 Hz

Uses Chebyshev implementation for steeper roll-off unity-gain, 2nd order, low-pass filter

Adding a separate filter for each channel increases system response time if an analog multiplexer is used

Figure 74. 3-Decade Logarithmic ADC Converter

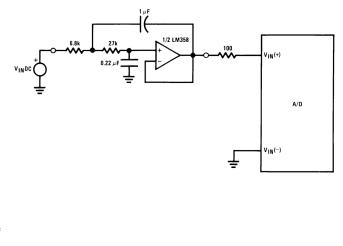


Figure 75. Noise Filtering the Analog Input



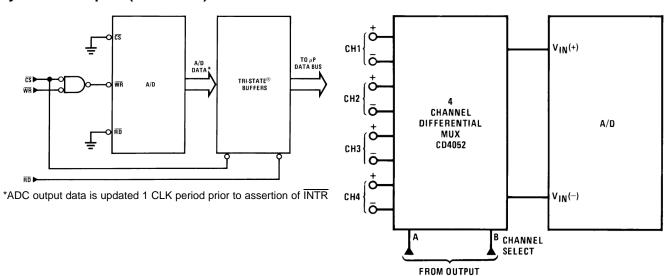
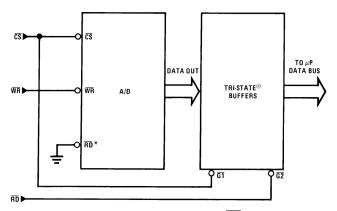


Figure 76. Output Buffers With ADC Data Enabled



*Allows output data to set-up at falling edge of CS

Figure 78. Increasing Bus Drive and/or Reducing Time on Bus

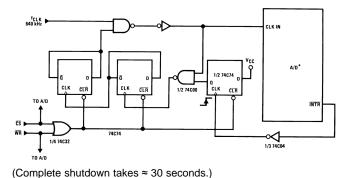
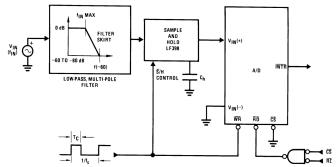


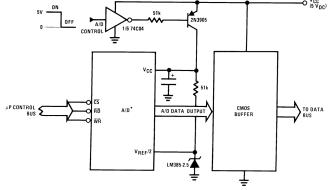
Figure 77. Multiplexing Differential Inputs

PORT OR μ P



(2) Consider the amplitude errors which are introduced within the passband of the filter.

Figure 79. Sampling an AC Input Signal



Buffer prevents data bus from overdriving output of ADC when in shutdown mode.

Figure 81. Power Savings by ADC and V_{REF} Shutdown

Figure 80. 70% Power Savings by Clock Gating



10 Power Supply Recommendations

Precautions should be taken to insure that the power supply for the integrated circuit never becomes reversed in polarity or that the unit is not inadvertently installed backwards in a test socket as an unlimited current surge through the resulting forward diode within the device could cause fusing of the internal conductors and result in a destroyed unit.

Noise spikes on the V_{CC} supply line can cause conversion errors as the comparator will respond to this noise. A low-inductance, low-ESR tantalum bypass capacitor should be used close to the converter VCC pin, and a 10- μ F is recommended. If an unregulated voltage is available in the system, a separate 5-V voltage regulator for the converter (and other analog circuitry) will greatly reduce digital noise on the V_{CC} supply.

11 Layout

11.1 Layout Guidelines

All logic signal wires and leads should be grouped and kept as far away as possible from the analog signal leads. Exposed leads to the analog inputs can cause undesired digital noise and 60-Hz pickup. Shielded leads for the analog inputs may be required in sensitive applications. A single-point analog ground should be used that is also separated from the logic ground points. The power supply bypass capacitor should be returned to digital ground. Any V_{RFF}/2 bypass capacitors, analog input filter capacitors, or input signal shielding should be returned to the analog ground point. A test for proper grounding is to measure the zero error of the ADC converter. Zero errors in excess of 1/4 LSB is generally traceable to improper PCB layout and/or wiring.

To minimize potential offset issues, TI recommends to route the signal traces differentially next to each other so that they will see the same thermal gradients and the same number of feedthroughs. Furthermore, inductance is determined by the size of the loop of current. Providing a path for return currents next to the signal trace will reduce the inductance. A solid ground plane is very advantageous in this regard. Ensure to minimize the loop area formed by the bypass capacitor connection between V_{CC} and ground. The ground pin should be connected to the PCB ground plane at the pin of the device.



12 Device and Documentation Support

12.1 Related Links

The table below lists quick access links. Categories include technical documents, support and community resources, tools and software, and quick access to sample or buy.

Table 4. Related Links

PARTS	PRODUCT FOLDER	SAMPLE & BUY	TECHNICAL DOCUMENTS	TOOLS & SOFTWARE	SUPPORT & COMMUNITY
ADC0801	Click here	Click here	Click here	Click here	Click here
ADC0802	Click here	Click here	Click here	Click here	Click here
ADC0803	Click here	Click here	Click here	Click here	Click here
ADC0804	Click here	Click here	Click here	Click here	Click here
ADC0805	Click here	Click here	Click here	Click here	Click here

12.2 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

TI E2E™ Online Community T's Engineer-to-Engineer (E2E) Community. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

Design Support *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

12.3 Trademarks

E2E is a trademark of Texas Instruments.

All other trademarks are the property of their respective owners.

12.4 Electrostatic Discharge Caution



These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

12.5 Glossary

SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.

13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

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22-Dec-2017

PACKAGING INFORMATION

Orderable Device	Status	Package Type	Package Drawing	Pins	Package Qty	Eco Plan	Lead/Ball Finish	MSL Peak Temp	Op Temp (°C)	Device Marking	Samples
ADC0802LCN/NOPB	LIFEBUY	PDIP	NFH	20	18	Green (RoHS & no Sb/Br)	CU SN	Level-1-NA-UNLIM	-40 to 85	ADC0802LCN	
ADC0802LCWM/NOPB	ACTIVE	SOIC	DW	20	36	Green (RoHS & no Sb/Br)	CU SN	Level-3-260C-168 HR	0 to 70	ADC0802 LCWM	Samples
ADC0803LCN/NOPB	LIFEBUY	PDIP	NFH	20	18	Pb-Free (RoHS)	CU SN	Level-1-NA-UNLIM	-40 to 85	ADC0803LCN	
ADC0804LCN	LIFEBUY	PDIP	NFH	20	18	TBD	Call TI	Call TI	0 to 70	ADC0804LCN	
ADC0804LCN/NOPB	LIFEBUY	PDIP	NFH	20	18	Green (RoHS & no Sb/Br)	CU SN	Level-1-NA-UNLIM	0 to 70	ADC0804LCN	
ADC0804LCWM	LIFEBUY	SOIC	DW	20	36	TBD	Call TI	Call TI	0 to 70	ADC0804 LCWM	
ADC0804LCWM/NOPB	ACTIVE	SOIC	DW	20	36	Green (RoHS & no Sb/Br)	CU SN	Level-3-260C-168 HR	0 to 70	ADC0804 LCWM	Samples
ADC0804LCWMX	LIFEBUY	SOIC	DW	20	1000	TBD	Call TI	Call TI	0 to 70	ADC0804 LCWM	
ADC0804LCWMX/NOPB	ACTIVE	SOIC	DW	20	1000	Green (RoHS & no Sb/Br)	CU SN	Level-3-260C-168 HR	0 to 70	ADC0804 LCWM	Samples

⁽¹⁾ The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

⁽³⁾ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

⁽⁴⁾ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.



PACKAGE OPTION ADDENDUM

22-Dec-2017

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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PACKAGE MATERIALS INFORMATION

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TAPE AND REEL INFORMATION





	Dimension designed to accommodate the component width
	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



*All dimensions are nominal

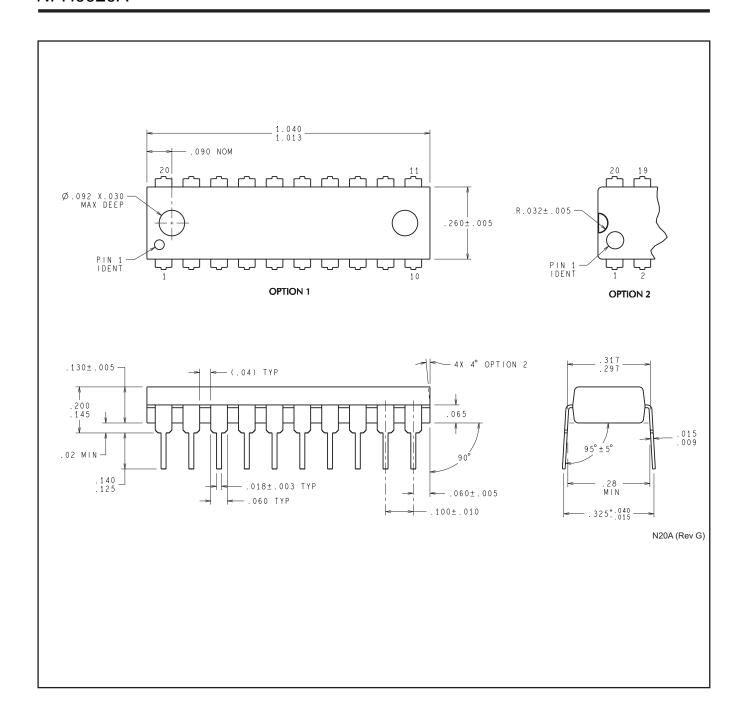
Device	Package Type	Package Drawing		SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
ADC0804LCWMX	SOIC	DW	20	1000	330.0	24.4	10.9	13.3	3.25	12.0	24.0	Q1
ADC0804LCWMX/NOPB	SOIC	DW	20	1000	330.0	24.4	10.9	13.3	3.25	12.0	24.0	Q1

www.ti.com 8-Apr-2015



*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
ADC0804LCWMX	SOIC	DW	20	1000	367.0	367.0	45.0
ADC0804LCWMX/NOPB	SOIC	DW	20	1000	367.0	367.0	45.0





SOIC



NOTES:

- 1. All linear dimensions are in millimeters. Dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.

 2. This drawing is subject to change without notice.

 3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not
- exceed 0.15 mm per side.
- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.43 mm per side.
- 5. Reference JEDEC registration MS-013.



SOIC



NOTES: (continued)

6. Publication IPC-7351 may have alternate designs.

7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SOIC



NOTES: (continued)

- 8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 9. Board assembly site may have different recommendations for stencil design.



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